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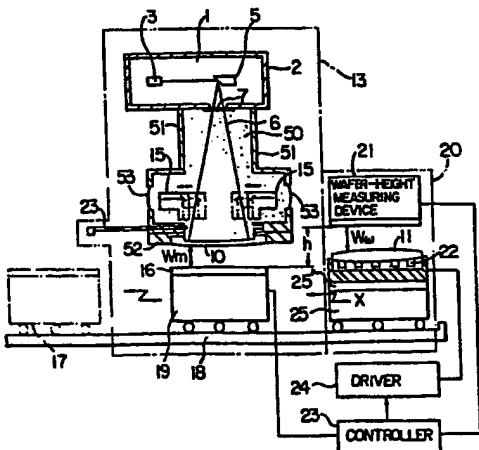
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54 Exposure process for transferring a mask pattern to a wafer.

67 An X ray exposure process and system for transferring a mask (10) pattern (9) onto a wafer (11) with use of X ray, wherein heights on the mask at many points are measured on a light interference band basis by a mask-height measuring device (16) of non-contact measurement type at an X ray exposure position (13), said mask being mounted on a chamber (51) which is filled with a He gas and the like to prevent attenuation of an X ray source (14), heights on the wafer at many points are measured at a wafer-height measuring position different from said exposure position, and according to the measured results, the wafer is finely moved upward or downward (that is, deformed) individually independently by means of a chuck (22) which sucks and holds the wafer at many points thereon, whereby a gap (S') between the mask and wafer is adjusted to a desired level (S).

FIG. 4



## EXPOSURE PROCESS AND SYSTEM

1        The present invention relates to an X-ray exposure process and system of forming a predetermined pattern provided in a mask on such a substrate as a silicon wafer, bubble wafer, ceramic substrate or  
5        printed circuit substrate with use of X rays.

      A recent demand for highly integrated semiconductor circuit requires a finer or accurater pattern fabrication. In the state of the art, a 1 or 2 micron pattern can be obtained by the photolithographic process,  
10      for example, by the ultraviolet ray-exposure process of reflection or reduction projection type. In order to obtain an even more integrated semiconductor circuit, a 1 micron or less pattern, so-called submicron pattern is necessary. However, it is difficult to obtain a  
15      high-resolution projection image by the conventional photolithographic process, because the process involves undesirable problems such as optical diffraction, multi-reflection and interference. Recent researches have developed an X-ray exposure process based on soft  
20      X rays having wavelengths between about 4 and 14  $\text{\AA}$  in order to eliminate the above problems.

      Explanation will first be directed to the principle of the known X-ray exposure process with reference to Fig. 1.

25      In operation, when electron beams 4 emitted

1 from an electron gun 3 are accelerated and directed to  
a target 5 within a vacuum chamber 2 which is  
kept therein at a high vacuum level (below  $10^{-6}$  Torr),  
characteristic X rays 6 depending upon the material of  
5 the target are radiated from the target 5. The X rays  
6 are emitted from the chamber 2 through a window 7  
mounted thereon. The window 7 can pass or transmit,  
for example, beryllium(Be) X rays alone. The rays 6  
are then projected from the window 7 via a mask 10 onto  
10 a resist 12 which is coated on a wafer 11 and reacts  
with the X rays 6. After exposed to the X rays 6,  
the resist 12 on the wafer 11 is developed to thereby  
transfer a pattern 9 onto the wafer 11. The mask 10  
comprises a mask carrier or base 8 made of a material  
15 (for example,  $\text{SiO}_2$ ,  $\text{Al}_2\text{O}_3$  or the like) permeable to  
X rays, and the pattern 9 carried on the carrier 8 and  
made of an X-ray absorbing metal such as gold. In  
this system, the use of soft X rays with short (4 to  
14  $\text{\AA}$ ) wavelengths causes less diffraction and scattering  
20 due to dusts on the wafer 11, allowing a highly accurate  
transfer of the fine or complicated pattern on the  
wafer.

Since it is practically difficult to obtain  
a flux of parallel X rays in the X-ray exposure system,  
25 X ray flux radiated from the target 5 is usually used.  
For this reason, the pattern 9 on the mask 10 is  
transferred on the wafer 11 in a distance "b"-offset  
positional relationship. The pattern offset amount "b"

1 is given as  $b = S \frac{W}{2D}$ , where D denotes a distance from  
the electron beam gun 5, S denotes a gap between the  
mask 10 and the wafer 11, and W denotes an effective  
mask diameter (dimension between the outermost ends  
5 of the pattern). Further, since the X rays 6 are emitted  
from the target 5 corresponding to the spot diameter  
"d" of the electron beams, the pattern 9 on the mask 10  
is transferred on the wafer 11 with an out-of-focus  
or defocus amount C. The out-of-focus quantity C is  
10 geometrically calculated as  $C = S \frac{d}{D}$ .

In order to transfer a very fine (submicron)  
pattern on a wafer with use of the X ray exposure system,  
the out-of-focus amount C must be adjusted below 0.1  
microns. On the other hand, the absolute value of the  
15 pattern offset "b" does not provide effect directly  
on the transfer accuracy, but variations in the offset  
"b" from one lithograph to another must be in the range  
of  $\pm 0.1 \mu\text{m}$ .

If the spot diameter "d" of the electron  
20 beams 4 is 3 mm, the distance D from the X ray source  
5 to the mask 10 is 300 mm, the effective mask diameter  
W is 75 mm and the permissible out-of-focus amount C  
of the pattern 9 is 0.1 microns, then the gap S between  
the mask 10 and the wafer 11 is 10 microns. In order  
25 to make  $\pm 0.1$  microns variations in the pattern offset  
"b", variations in the gap S must be in the range of  
 $\pm 0.8$  microns (about  $\pm 1$  micron).

The X ray exposure system so far suggested at

1 its experiment and research level, has a difficulty  
that, as shown in Fig. 2, the gap S between the mask 10  
and the wafer 11 is not constant, because the thin and  
weak mask 10 tends to deform or distort highly, which  
5 makes difficult it to transfer the pattern with a high  
accuracy.

More specifically, in the suggested X ray  
exposure system, the mask carrier or base 8 is made of  
material permeable to the X rays 6, for example, macro-  
10 molecular material such as  $\text{SiO}_2$ ,  $\text{Al}_2\text{O}_3$  and polyimide,  
and is of thin film having a thickness of several  
microns to several tens microns. Therefore, the mask  
10 is weak in strength and tends to deform under varying  
environmental pressure and temperature. And this  
15 tendency of the mask 10 becomes remarkable as the mask  
is made larger, which has, so far, hindered the develop-  
ment of an X ray exposure system on a batch basis.

On the other hand, the wafer 11 has a thickness  
of about 200 microns and thus relatively thick and  
20 less in deformation and distortion, when compared with  
the mask 10. While, the wafer 11 has a evenness or  
flatness of usually above 4 microns and sometimes  
 $\pm 10$  microns. However, it is practically difficult to  
enhance the flatness of the wafer 10 in the current-level  
25 wafer production process.

As has been explained above, the conventional  
system has a difficulty that the submicron pattern can  
not be transferred onto the wafer with high accuracy,

1 since the gap  $S$  between the wafer 11 and mask 10  
varies in the range of  $\pm$  several tens microns or  
above and since the offset "b" and out-of-focus  $C$  of  
the pattern vary each time the wafer is exposed to X  
5 rays through the mask 10.

It is an object of the present invention to  
provide an X-ray exposure process and system which has  
eliminated the above defects in the prior art, and  
wherein the wafer is deformed according to the mask  
10 shape so as to keep constant the gap or spacing between  
the wafer and mask and under this condition, the mask  
pattern is X-ray transferred on the wafer, thereby  
enhancing the yield in production of semiconductor,  
magnetic bubble, thick or thin film circuit or printed  
15 circuit substrate.

In order accomplish the above object, according  
to the present invention, a pattern exposure station and  
a wafer-height measuring station are separately provided  
so as to allow a mask-height measuring device placed on  
20 a movable stage to measure heights on the mask surface  
at many points at the exposure station and also to  
allow a wafer-height measuring device to measure  
heights on the wafer surface at many points at the  
wafer-height measuring station, whereby the wafer is  
25 deformed according to the measured results by means of  
a wafer deforming mechanism so that the gap between the  
mask and wafer is constant or uniform when the mask is  
placed on the wafer. The wafer deforming mechanism

1 functions to finely move or displace the wafer upward  
or downward by means of a chuck which sucks and holds  
the wafer at its plural points individually independently.

Next, the mask-height measuring device is  
5 moved backward from the exposure station and instead  
the wafer stage including the wafer deformor mechanism  
is moved toward the exposure station, and then the  
wafer is exposed to X rays through the mask to thereby  
transfer a predetermined pattern on the wafer.

10 The X ray exposure system according to the  
present invention is characterized in that a chuck  
comprises a plurality of displacement generating means  
for independently finely moving the wafer upward or  
downward at plural positions thereon and means for  
15 sucking and holding the wafer on the upper surface  
of said displacement generating means, and that the  
wafer is deformed according to the mask shape so as to  
maintain the spacing between the mask and wafer at a  
desired value and thereby to transfer the mask pattern on  
20 the wafer by exposing the wafer to X rays.

The above and other objects and advantages  
of the present invention will become clear from the  
following description with reference to the accompanying  
drawings, in which:

25 Fig. 1 is a diagram showing the principle of  
the X ray exposure process;

Fig. 2 is a diagram showing a gap relationship  
between a mask and a wafer used in a prior art system;

1       Fig. 3 is a diagram showing a gap relationship  
between a mask and a wafer used in the present invention;

5       Figs. 4 and 5 are diagrams showing an X ray  
exposure process and system in accordance with the  
invention;

Fig. 6a is a plan view of an embodiment of a  
wafer deforming device in accordance with the invention;

Fig. 6b is a cross-sectional view of the device  
of Fig. 6a;

10       Fig. 7a is a plan view of another embodiment  
of the wafer deforming device in accordance with the  
invention;

Fig. 7b is a cross-sectional view of the device  
of Fig. 7a;

15       Fig. 8 is a plan view of an embodiment of a  
wafer-height measuring device in accordance with the  
invention;

Fig. 9 is a front view of the device of Fig. 8;

20       Fig. 10 is a schematic diagram of the signal  
processing circuit of device of Fig. 8;

Fig. 11 is a perspective view of an embodiment  
of a mask-height measuring device in accordance with  
the invention;

25       Fig. 12 is a schematic arrangement of the  
device of Fig. 11; and

Fig. 13 is a detailed arrangement of an  
alignment scope used to measure a gap between the mask  
and wafer at a alignment target mark position.

1 An X ray exposure process and system according  
to the present invention will be detailed. The principle  
of the X ray exposure process is as shown in Fig. 1.  
As has been explained earlier in connection with the  
5 prior-art X ray exposure process, it is difficult, in  
the prior art, to maintain constant the gap S between  
the mask 10 and wafer 11 as shown in Fig. 2, since  
the mask 10 tends to deform or warp and the thickness  
tolerance of the wafer 11 varies. A major feature of  
10 the present invention is to deform the wafer 11 according  
to the shape of the mask 10 to thereby make constant  
the gap S between the wafer and mask, as illustrated  
in Fig. 3.

There is shown an embodiment of the X ray  
15 exposure process according to the invention in Figs.  
4 and 5 wherein the mask 10 and a position detector or  
alignment scope 15 (which will be described later) for  
aligning the wafer 11 with the mask 10 are provided  
below an X ray source 14 in the X ray exposure station  
20 13.

More specifically, the electron gun 3 and the  
target 5 are as an X-ray generating source placed within  
the vacuum chamber 2 which is kept therein at a high  
vacuum level (below  $10^{-6}$  Torr). On the vacuum chamber  
25 2 near the target 5 is mounted the window 7 through  
which the X rays 6 are emitted from the chamber 2  
into another atmosphere (He atmosphere) 50.

In a practical system, generally, the target 5

1 is of water-cooled and rotary type in order to obtain strong X rays. Further, the target 5 is often made of metal such as Al, Si or Pd. In this case, the radiated X rays have wavelengths between 8 and 4 Å.

5 The window 7 must be able to bear or withstand a pressure difference 760 Torr (about 1.0 kg/cm<sup>2</sup>) between the vacuum chamber 2 and a He chamber 51, and at the same time must be made of material permeable to X rays. The window 7 may be approximately between 2  
10 and 3 cm<sup>2</sup> in its area and may be of thin Be film of 25 microns or less in thickness so long as the window is disposed near the target 5, which is enough to withstand the pressure difference between the chambers.

Since such a thin film can be used as the  
15 window 5, this can also reduce the attenuation factor of the X ray. The X rays 6 passed through the window 7 are directed to the wafer 11 via the pattern of the mask 10 which is attached directly to the lower end of the He chamber 51. The chamber 51 is filled with a  
20 He gas, etc. and kept at an atmospheric pressure (760 Torr). The mask 10 is deformable and has a thickness of several μm. The mask also comprises a carrier or base 8 made of SiO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub> and the like permeable to X ray and a circuit pattern 9 made of such X-ray absorbent  
25 material as gold. The mask is removably attached to the lower end of the chamber 51 with the mask engaged with a mask holder 52.

In order to allow an X-ray transfer of a lot

1 of wafers 11 with use of a single piece of mask 10 and correspondingly raise its throughput remarkably, the mask 10 must be aligned accurately with the pattern of wafer 11 with the mask mounted on the lower end of the chamber 5 51. For this purpose, the wafer 11 is fixed on a wafer table 25 in a relation a very-small-spacing S spaced from the mask 10. When the wafer 11 is spaced such a small gap from the mask 10, the X ray attenuation is 0.1% and thus can be neglected.

10 The alignment scope 15 is disposed to allow its horizontal movement and achieve alignment between the mask 10 and wafer 11. Alternatively, since the alignment scope 15 containing therein optical and image elements (linear image sensors) and/or image devices 15 and the like may be sealed, a portion of the scope 15 may be disposed outside of the chamber 51, if necessary. The wafer 11 is comprised of a wafer substrate coated thereon with resist. In order to achieve a proper alignment between the wafer 11 and mask 10, a wafer 20 stage 25' is provided in the wafer table 25 to allow X, Y, Q and Z direction movements for fine or coarse adjustment. Reference numeral 53 is a diaphragm.

On the other hand, a mask-height measuring device 16 is built in the stage 19 to allow movement 25 from the X ray emitting station 13 to a standby position 17, and functions to measure heights  $W_m$  of the mask 10 at a plurality of points in the station 13. The stage 19 in turn slidably moves along a straight guide rail 18

1 accurately. Also, a wafer-height measuring station 20  
is provided next to the X ray emitting station 13, and  
a wafer-height measuring device 21 in the station 20 is  
used to measure heights  $W_w$  of the wafer 11 at a plurality  
5 of points. The wafer 11 is sucked and held by a wafer  
deforming chuck 22. A controller 23 calculates the  
gaps  $S$  between the mask and wafer on the basis of the  
mask heights  $W_m$  and wafer heights  $W_w$  measured at the  
corresponding points thereof, and instructs a wafer  
10 height compensation amount  $\Delta W_w$  to a drive controlling  
section 24 so that the gaps  $S$  become constant at the  
respective points of the mask and wafer. According to  
the instruction data, the drive controlling section 24  
provides corresponding compensation inputs for a  
15 plurality of wafer deforming chucks 22 and deforms  
the wafer 11.

The wafer height compensation  $\Delta W_w$  is given as  
$$\Delta W_w = (S + h) - (W_m + W_w)$$
, where "h" is a height difference  
between the reference surfaces of the mask-height and  
20 wafer-height measuring devices and  $S$  is a set gap between  
the mask and wafer. However, it will be understood  
that the calculation procedure is different depending  
on the different measuring method and the different  
setting of the measuring references and thus does not  
25 need to always follow the above calculation equation.

The wafer deforming chuck 22 is provided on  
the wafer feed or movement stage 25 and thus are moved  
toward the X ray exposure station 13 along the straight

1 guide rail 18. On the other hand, as has been described  
in the foregoing, the mask-height measuring device 16  
is moved toward the standby position 17 by the stage 19  
which carries the device 16, after measuring the mask  
5 height. Fig. 5 shows the state when the X ray exposure  
process and system of the invention shown in Fig. 4 is  
in its X-ray exposure mode.

The wafer movement stage 25 which moves the  
wafer 11 into the X ray exposure station 13, also  
10 contains therein the Y, Q and Z movement mechanism 25' as  
a wafer-position adjusting mechanism for position alignment  
between the wafer 11 and the mask pattern. The alignment  
scope 15 is moved and positioned above the mask 10 before  
X ray exposure. After aligned with the wafer movement  
15 stage 25 for pattern alignment, the scope 15 is moved up  
to the standby position to avoid the blockage of X ray  
passage by the scope and allow the proper exposure of  
the wafer to X rays.

On the other hand, the wafer 11 can be deformed  
20 in the following two manners. That is, the heights of  
the mask 10 and wafer 11 are measured and according to  
the measured results, the wafer 11 is deformed at the  
wafer-height measuring station 20. The measured mask  
and wafer heights are pre-stored and according to the  
25 stored data, the wafer 11 is deformed at the X ray exposure  
station 13. These two manners can be selected according  
to the system's controlling requirements.

Next, the wafer deforming procedure and the

1 structure of the wafer deforming chuck 22 will be  
explained with reference to an embodiment of the present  
invention.

Figs. 6a and 6b shows an embodiment of the wafer  
5 deforming chucks wherein the wafer 11 is conformed to  
the shape of the mask 10 by moving upward or downward  
up/down elements in the chuck and deforming the wafer.  
Figs. 6a and 6b are a plane view and cross-sectional  
view, respectively, of the detailed structure of the  
10 wafer deforming device. For one of the gratings divided  
as shown in Fig. 6a, an up/down displacement unit 36  
is provided which comprises a motor 33, a gear 34, and  
an up/down element 35 having feed screw, as shown in  
Fig. 6b. The wafer deforming chuck device shown in  
15 Figs. 6a and 6b has the separately driven up/down  
displacement units 36, the wafer-height measuring units  
21 provided for the respective displacement units 36,  
a chuck body 38 contained therein with the displacement  
units 36 for sucking and holding the wafer 11, a piping  
20 37 communicated with a vacuum piping (not shown) for  
putting the inside of the chuck body under vacuum, the  
controller 23 used to calculate all the measured wafer-  
height and mask-height values and determine the up/down  
amount  $\Delta W_w$  for each of the up/down displacers 36, and  
25 the drive controlling section or driver 24 for driving  
the motors 33.

The wafer 11 is vacuum attracted in such a  
manner that the wafer follows or conforms to the tip ends

1 of the up/down displacement units 36, and thus the wafer  
surface can be moved or displaced upward or downward  
locally by selectively actuating the respective units 36.

After the measurement of the wafer-height and  
5 mask-height, the motors 33 rotates respectively by  
amounts corresponding to respective correction  $\Delta W_w$  to  
thereby move upward or downward the up/down elements  
or feed screw 35 via the reduction gears 34 through  
which the rotational movement of the motor is reduced.

10 In the case where a DC motor is used as the motor 33,  
the reduction ratio of reduction gear 34 must be as  
large as 10,000 : 1 to 100,000 : 1. On the other hand,  
when a pulse motor is used as the motor 33, the gear  
reduction ratio can be small enough to be able to control  
15 the up/down element 35 for every approximately 0.5  
micron increments or decrements, without any need for  
such a large gear ratio as in the case of DC motor.  
Further, the use of the DC motor facilitates an up/down  
amount control by the detector 21 in a closed loop,  
20 whereas the use of the pulse motor allows an open loop  
control. The DC motor is disadvantageously larger in  
size and provides more heat even during its stoppage  
than the pulse motor. In either case of the DC and  
pulse motors, backlash or play must be eliminated or  
25 suppressed to a controllable or permissible level.

In short, the wafer deforming chuck 22 has a  
plurality of up/down elements 35 at its upper side  
and the elements 35 can be separately displaced upward

1 or downward by the respective up/down displacement units 36 to allow fine adjustment.

Also, the displacement units 36 may be replaced not only the above-mentioned screws coupled to the motors 5 but also by piezoelectric elements, mangetostrictive elements, thermally deforming elements, magnet- or fluid-based units, fine displacement mechanism based on lever, or combination thereof. In the case of semiconductor wafer, the stroke of the displacement unit 36 must be 10 30 microns, the positioning accuracy must be below  $\pm 1$  micron, the deformation rate must be faster than the throughput rate, and the wafer must be stable during its X ray exposure.

As disclosed in Fig. 7 in USP Serial No.

15 245,193 filed in March 18, 1981, a thin film 56d may be applied over the displacing devices 36. A structure of the thin film 56d will be described later. The displacing device 36 may comprise a member 36a bonded to the bottom surface of the thin film 56d, a U-shaped 20 member 36c which is clamped to the chuck body 38 and can be level-adjusted by a screw 36d, a member 36d clamped to the member 36c, a piezoelectric element 36e having its lower end fixed to the member 36d, a ball 36f disposed between the upper end of the piezo- 25 electric element 36e and the lower end of the member 36a and a spring 36g for tensioning the memeber 36a and the member 36d. A sphere 38a is mounted on the bottom surface of the chuck body 38. A stage 56s which supports the

1 sphere 38a of the chuck body 38 by a spherical seat 56u  
is movable upward and downward by a lead screw mechanism,  
not shown. Since the substrate 11 is deformed through  
the thin film 56d while the substrate 11 is sucked and  
5 held by the thin film 56d, no localized stress is  
applied to the substrate 11 and the breaking of the sub-  
strate is prevented and the exposure surface of the sub-  
strate 11 can be smoothly deformed to conform to a  
desired shape.

10 In an alternative of the displacing device  
36, vacuum pressures to a plurality of chambers may be  
adjusted to deform the thin film 56d in the shape of  
diaphragm. Numeral 56g shows a bore through which  
the substrate 11 is sucked to the thin film 56d.

15 The substrate deformation measuring device 21  
may be of contact type or non-contact type. The contact  
type includes a dial gauge device and the non-contact  
type includes an air micrometer, electromagnetic device,  
static capacitance device and optical device. The  
20 substrate deformation correcting thin film 56d is made  
of a thin, flexible metal plate such as steel, aluminum,  
stainless steel, phosphor bronze or silicon, having a  
thickness of 0.4 - 3 mm, a thin glass plate having a  
thickness of approximately 0.7 mm, or a thin resin  
25 plate such as Tefuron. It has a ring-shaped ribs 56e  
of approximately 50 - 100  $\mu\text{m}$  height around an outer  
periphery thereof and regularly arranged within the  
outer periphery. A chuck body 38 having a flexible

1 wafer chuck surface 56d integrally fixed to the upper  
end of a cylinder 56b is mounted inside the rib 56e.  
The rib 56e may be of square shape or circular shape.  
In order to support the periphery of the wafer chuck  
5 surface 56d substantially freely, a ring-shaped groove  
56z is formed to reduce the thickness. In order to  
eject the exposed wafer 11 by an air jet force, an  
obliquely oriented transport hole 56g is formed. The  
hole 56g is connected to a room 56x formed in the chuck  
10 body 38. The path 56x is connected to a vacuum source  
49 through a flexible pipe 56w.

The wafer-height and mask-height measuring  
devices are each classified into contact type and non-  
contact type. A typical example of the contact type  
15 measuring devices is a dial gauge, but it is not suitable  
for mask-height measurement applications because the  
mask 10 is thin and tends to easily deform. On the other  
hand, the non-contact type measuring devices include,  
for example, an air micrometer, an electromagnetic  
20 instrument, an electrostatic capacity type instrument,  
an optical instrument, an ultrasonic-wave based instru-  
ment.

An example most preferable as the wafer-height  
measuring device 21 is disclosed in USP Serial No.  
25 292,933 (filed in August 14, 1981) herein as Figs. 8 to  
10. The example will be explained below with reference  
to Figs. 8 to 10. Referring now to Fig. 9, the wafer  
deforming chuck 22 mounted on the wafer feed stage 25

1 is supported slidably in an arrow d direction 129 by air bearings 128 rested on the straight guide rail 18. The deformation amount of the wafer 11 surface is detected and stored at the wafer-height measuring station 20.

5 As illustrated in Fig. 9, a disc 123 is disposed in parallel with the wafer 11. The disc 123 is carried on the straight guide rail 18 through air bearing 128. The upper surface of the straight guide rail 18 and the lower surface 123a of the disc 123, 10 contacting with the steel balls 124, are carefully and precisely flattened. The base 131, circular in shape, is fixed on. Accordingly, the disc 123 continues its rotation in a fixed direction, being precisely kept parallel to the wafer 11, by means of the combination of 15 the base 131, the steel balls 124 and the rotating bearings 132.

The disc 123 is provided with a plurality of detecting probes 60 directed at their tips toward the surface of the wafer 11 for detecting distances from the 20 tips thereof to the surface of the wafer 11.

The plurality of detecting probes 60 mounted to the disc 123 are arranged in a linear or curved fashion from the center of the disc 123 to the peripheral portion thereof.

25 The detecting signals from the detecting probes 60 are led out through cables 133. The cables 133 are fixed to a rotating side 134 of a slip ring which is held by the disc 123 and moves together with the disc

- 1 123. The detecting signals further travel from a stationary side 135 of the slip ring which is held by a holder frame 137 fixed to the spacers 130, through a cable 136, to a signal processing means containing a
- 5 display, an arithmetic unit, a CRT and the like. The signal from the cable 136 is an analog signal produced through one revolution of the disc 123. For the signal processing, the analog signal may directly be used for representing the flatness information of the wafer 11.
- 10 Alternately, the analog signal may be converted, every given rotational angle of the disc 123, into a digital signal which is used as the flatness information of the wafer 11. In any case of using a digital or analog signal, it is desirable to provide means for detecting
- 15 rotation position of the disc 123. The disc 123 in Fig. 9 is additionally provided with means for detecting timings to perform the A/D conversion, that is to say, for finding measuring locations on the wafer 11, i.e. rotation positoin of the disc 123. To be more specific,
- 20 a plurality of marks 142a, 142b, ... are sticked around the lower portion of the shoulder 123b of the disc 123, being arranged equidistantly. When the A/D conversion is performed every 1/16 revolution of the disc 123, sixteen marks 142a, 142b, ... 142p are sticked
- 25 to the lower shoulder portion every rotation of 22.5°. In this case, the passage of the mark is sensed by a photosensor 143 shown in Fig. 8 and an output signal from the photosensor is used as a timing signal for

- 1 the A/D conversion or the measuring position data for the wafer 11. If one of the sixteen marks is longer than the remaining ones, a signal representing a rotation start or an origin of the timing signal can be
- 5 obtained from the longer mark.

Circuit diagram for processing output signals from the detecting probes 60 in synchronism with timing signal obtained by the photosensor 143 to obtain the degree of flatness of the wafer 11 will be explained

- 10 referring to Fig. 10. Fig. 10 shows an example in which three electrostatic capacitor type sensors are used as the detecting probes 60. In Fig. 10, reference numeral 46 shows current-voltage converting amplifiers each for converting output current from the corresponding
- 15 detecting probe 60 into a current signal, and 148 shows an analog-digital converter for converting analog voltage signals from the amplifiers 46 into digital signals in response to a timing signal from the photosensor 143. The digital output signal of the A/D converter 148 is
- 20 applied to a signal processor including a CPU (not shown) for calculating degree of flatness of the wafer 11.

In this way, the deformation amounts on the wafer 11 surface at many points are detected at the wafer-height measuring station 20. The detecting probe 60 may

- 25 be such an electrostatic capacity sensor as disclosed in USP Application No. 6,424,012. The deformation amounts on the wafer 11 surface can be detected by the sensor because the wafer 11 is grounded.

1         Detailed explanation will next be directed to  
how the mask-height measuring device 16 detects the  
deformation amounts on the easy-to-deform mask 10.  
Fig. 11 shows an arrangement or structure of the mask-  
5         height measuring device 16. In the figure, He-Ne  
laser rays emitted from a laser tube 201 are guided via  
reflection mirrors  $M_1$  and  $M_2$  to a deflection plate  
202 the rotation of which acts to change the intensity  
of the received laser rays. The laser rays intensity-  
10         adjusted at the deflection plate 202 are then entered  
in a beam expander 203 to form a laser beam having a  
spot diameter or size of 30  $\mu\text{m}$  on the mask 10. The  
laser beam exiting from the expander 203 is directed  
via a reflection mirror  $M_3$  into a prism 204. Inter-  
15         ference fringe of equal thickness appeared on the prism  
surface and the mask surface is imaged on the tube of  
a TV camera 206 through an imaging or focusing lens 205.  
Reference numerals  $M_4$  and  $M_5$  are also reflection mirrors.  
An electrostatic capacity sensor 207 is provided next  
20         to the prism 204 to detect the absolute value of the  
height corresponding to a point on partial conductive  
thin film formed in the periphery of the mask 10.

25         The prism 204 is supported by a spring set or  
leaf springs 208 to allow an fine up/down displacement.  
More particularly, the prism can be finely moved upward  
or downward by a piezo-electric element 209 having a  
maximum stroke of 25  $\mu\text{m}$ , as shown in Fig. 12.

Fig. 11 shows the basic principle of how the

1 interference fringe of equal thickness are developed or  
generated. The deformation amounts on the mask surface  
appear in the form of contour lines in the inter-  
ference bands, since the parallel laser rays in phase  
5 are interfered with their components reflected at the  
prism surface and their components reflected at the  
mask surface. The difference of distance between  
surfaces of the prism and the mask corresponding to  
positions at which contour lines in the interference  
10 bands exist is determined by the angle of incidence  
when the laser rays enter into the mask surface and  
the wavelength of the laser beam. The distance can  
varys from about 0.3  $\mu\text{m}$  to infinity ( $\infty$ ) in accordance  
with the change of the angle of incidence but is pre-  
15 ferably 2  $\mu\text{m}$ . In Fig. 12, a fine displacement or move-  
ment of the prism 204 upward or downward will cause a  
movement of the interference bands. Therefore, the  
prism 204 is mvoed stepwise every 0.125  $\mu\text{m}$  through a  
driver 210 which is actuated by a command from a  
20 controller 211, and the interference band image is  
entered into the TV camera 206. At the same time, the  
position of the prism and the position of the inter-  
ference band are stored in a memory in a microprocessor  
25 212. This procedure is repeated at 16 times by a  
mount corresponding to the interference band pitch 2  $\mu\text{m}$ .  
The deformation amounts on the mask 10 can be found by  
analyzing or calculating the positions of the prism  
and the positions of the interference band corresponding

1 to 16 times with use of the microprocessor 212. That  
is to say, in case the surface of the mask projects  
in the down direction, the interference fringe is  
moved in the radial direction when the prism 204 is  
5 moved upward. In case the surface of the prism is  
concave, the interference fringe is moved in the direc-  
tion of the center thereof. Therefore, the projection  
and the concavity of the mask can be distinguished by  
analyzing the movement direction of the interference  
10 fringe by the microprocessor. Moreover, when the prism  
204 is moved by 0.125  $\mu\text{m}$ , difference between the height  
of the mask surface corresponding to position at which  
an interference fringe exist before the movement of  
the prism and that after the movement of the prism  
15 corresponds to 0.125  $\mu\text{m}$ . Accordingly, the deformation of  
the mask can be measured with the precision of 0.125  $\mu\text{m}$ .  
The fundamental concept is known and is carried out in  
such a manner as disclosed in the SPIE, Vol. 135, pages  
104 to 110, entitled "The Interferometric Analysis of  
20 Flatness by Eye and Computer".

On the other hand, the mask deformation amounts  
obtained from the prism are relative difference but the  
absolute height values corresponding to the deformation  
amounts are unknown.

25 For this purpose of knowing the absolute  
heights, the electrostatic capacity sensor 207 is used  
to measure the absolute values  $W_{mA}$  of heights of the  
conductive thin film (for example Au) in the periphery

1 of the mask carrier or base 8 in which the LSI circuit pattern is not exist.

The absolute mask deformation value  $W_m$  is expressed as the following equation.

$$W_m = F(x, y) + \Delta \quad \text{----- (1)}$$

5 Where,  $\Delta$  is a constant necessary for a relative value  $F(x, y)$ . The absolute value  $F(x_o, y_o)$  at a point  $(x_o, y_o)$  measured by the sensor 207 is known with use of the prism,  $\Delta$  satisfies the following equation (2).

$$\Delta = W_{mA} - F(x_o, y_o) \quad \text{----- (2)}$$

10 In this way, the absolute deformation amount  $W_m$  on the entire mask 10 can be obtained from equation (1).

Although there has been explained in the foregoing a system wherein the absolute values of heights of the mask 10 are measured by the sensor 207 shown in 15 Fig. 11 and the absolute values of gaps between the wafer 11 and the mask 10 are adjusted to their desired levels, an alternative system may be used. That is, the deformation amounts of the mask 10 and wafer 11 are detected by the mask-height and wafer-height measuring 20 devices 17 and 21 based on light interference bands, and subsequently the wafer 11 is deformed by means of the wafer deforming chuck 19 so that the wafer conforms in shape to the mask 10. In this way, the wafer 11 has

- 1 been deformed so as to conform to the mask 10 in shape. And by aligning alignment marks 314 of the wafer 11 with alignment marks 315 of the mask 10 with use of the optical double-focus alignment system of Fig. 13, the
- 5 gap between the mask 10 and wafer 11 can be adjusted to a predetermined value S.

More specifically, the mask alignment marks 314 information is sent via an optical path A on the mask side (including an object lens 300, a beam splitter 301, 10 a rectangular prism 302 and a beam splitter 303) to a linear image sensor 313 where the marks 314 in the information are detected. By tilting the entire mask 10 with use of a piezoelectric element 308, the marks 314 are focused on the sensor 313.

15 On the other hand, a shorter light path B on the wafer side (including an object lens 300, a beam splitter 301, a mirror 306 and a beam splitter 303) is provided so that when the wafer alignment mark 315 is spaced a spacing S of about  $10 \mu\text{m}$  from the mask alignment 20 mark 314, the wafer mark 315 becomes focused on the linear image sensor 313. Therefore, the entire deforming chuck 22 is pre-adjusted so that the gap  $S'$  between the wafer 11 and mask 10 (at the mark 314 and 315 positions) is larger than the gap S. Next, the piezoelectric 25 element 309 for wafer tilting is moved gradually upward by a piezoelectric-element driver 310. Under this condition, a controller 311 detects the maximum of the output signal supplied from the linear sensor 313.

- 1 The entire deforming chuck 19 is positioned at the focused position detected by the controller. This results in that gap between the mask 10 and wafer 11 at the mark 314 and 315 positions becomes the predetermined value S.
- 5 As a result, there can be corrected a very small tilt in the wafer 11 which occurs when the wafer 11 is transferred from the wafer-height measuring device to the X ray exposure position by moving the wafer movement stage 25 mounted at its top with the wafer. In order to
- 10 detect the alignment marks 314 and 315, optical shutters 307 and 308 may be provided, if desired.

According to the present invention, as has been disclosed in the foregoing, the gap between the pattern transfer mask and wafer can be made always constant or uniform with accuracy within  $\pm 1$  micron even if the mask is deformed, waved or curved, by deforming the wafer so as to conform to the shape of the mask. As a result, the offset and out-of-focus (defocused) amounts b, c of the transfer pattern can be kept constant. For example, a submicron (below 1 micron) pattern can be accurately transferred onto the wafer with use of X rays. In addition, in photolithographic process, it is possible to transfer a fine pattern at its optical resolution limit, which leads to a remarkable improvement in the yield of such integrated circuit chips as LSI.

The mask-height measuring device 16 and the movement stage 25 have been supported slidably on the same straight guide rail 18 in the above embodiments,

- 1 it will be appreciated that the device and stage are carried preferably on different straight guide rails respectively because the wafer chuck 22 must be provided with a mechanism which supplies and discharges the wafer
- 5 10 in the practical applications. That is, it is desirable to support the mask-height measuring device 16 slidably on another straight guide rail which extends in a direction perpendicular to the paper plane of Fig. 4.

WHAT IS CLAIMED IS:

1. An exposure process for transferring a mask (10) pattern (9) on a wafer (11) wherein heights on the mask surface at many points are measured by a mask-height measuring device (16) and heights on the wafer surface at many points are measured by a wafer-height measuring device (21), so that the wafer is defomed by means of a chuck (35, 36, 38) which sucks and holds the wafer at many points thereon and finely moves the wafer upward or downward individually independently at said many points according to said measured results, whereby a gap (S') between the mask and the wafer is adjusted to a predetermined value (S).  
10
2. An exposure process as set forth in claim 1 wherein said exposure process is of X ray exposure type.  
15
3. An exposure system for transferring onto a wafer (11) a circuit pattern (9) formed on a mask (10), said system comprising a chuck (35, 36, 38) provided with means (35) for sucking and holding said wafer at many points thereon and finely moving the wafer upward or downward individually independently at said many points; a stage (19) provided with said chuck and supported slidably on a platen between an exposure position (15) and a wafer-height measuring position; a wafer-height measuring device (21) disposed opposed to the wafer moved in said wafer-height measuring position by said stage for measuring heights on the wafer at said many points; and a mask-height measuring device (16) slidably  
20  
25

supported on said platen between said exposure position and a standby position (17) and disposed opposed to the mask at the exposure position, for measuring heights on the mask surface at many points; wherein a gap between

5 the wafer and the mask is detected according to said wafer heights measured by said wafer-height measuring device and said mask heights measured by said mask-height measuring device, and wherein said fine up/down moving means (36) are actuated so that said detected

10 gap (S') becomes a predetermined value (S).

4. An exposure system as set forth in claim 3 wherein said exposure system is of X ray exposure type and includes an X ray source (14) and means (1, 2, 51, 50) for preventing the attenuation of X rays emitted from

15 said X ray source and for radiating the X rays on the mask (10).

5. An exposure system as set forth in claim 4 wherein said mask-height measuring device (16) includes an optical mask-height measuring means.

20 6. An exposure system as set forth in claim 5 wherein said optical mask-height measuring means measures said mask heights on light interference band basis.

7. An exposure system as set forth in claim 6

25 wherein said mask-height measuring device (16) includes a sensor (313) for detecting the absolute values of positions on the mask (10) and in the periphery thereof.

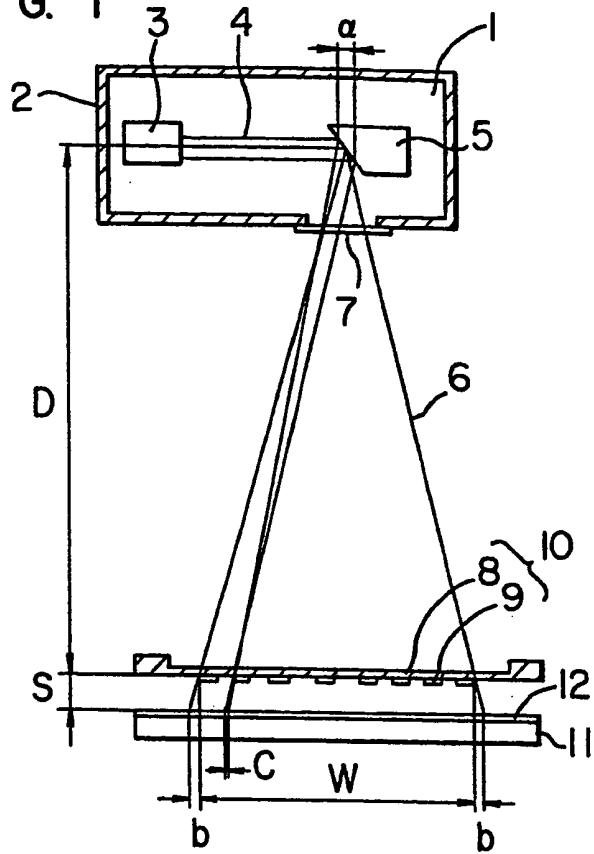
8. An exposure system as set forth in claim 6,

further including an observation or detection optical system (215) provided within a chamber for observing or imaging an alignment mark (314 or 315) on the mask and an alignment mark on the wafer and for detecting a gap 5 (S') between the mask (10) and wafer (11) at said alignment mark positions respectively on the mask and wafer, and means for finely moving said entire chuck (22) upward or downward in such a manner that said gap detected by said optical system becomes a predeter- 10 mined value (S).

9. An exposure system as set forth in claim 8 wherein said observation or detection optical system (215) includes a double focus optical system with different light paths (A, B).

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FIG. I



**FIG. 2**

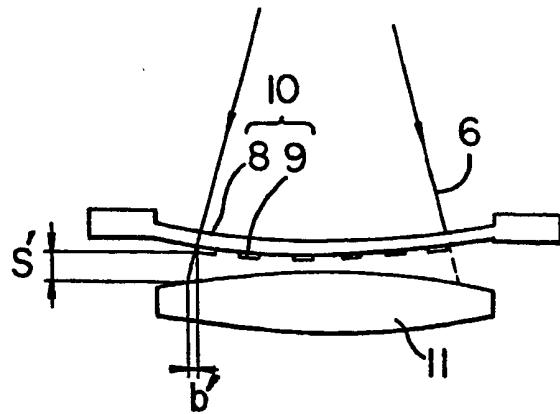


FIG. 3

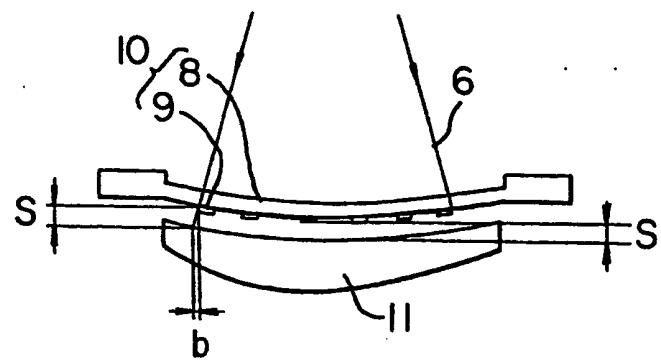


FIG. 4

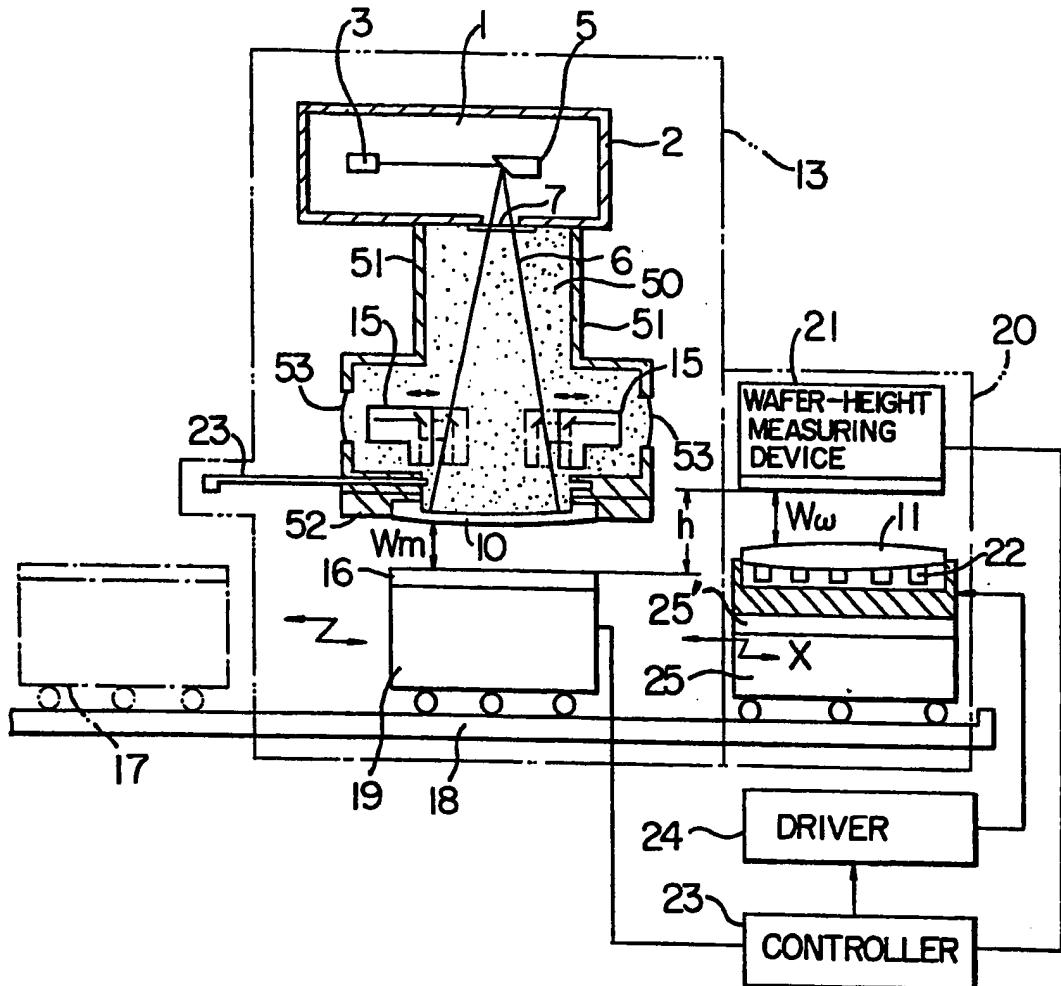
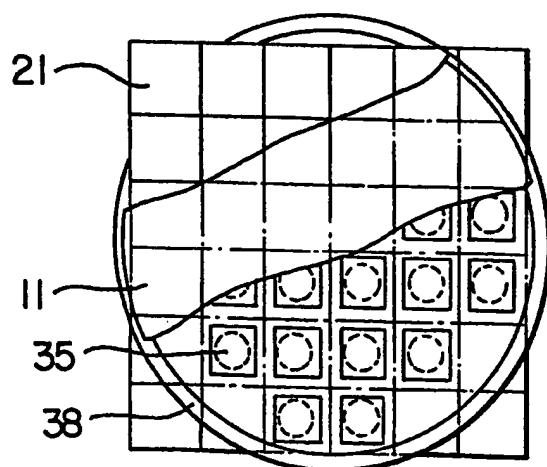


FIG. 6a



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FIG. 5

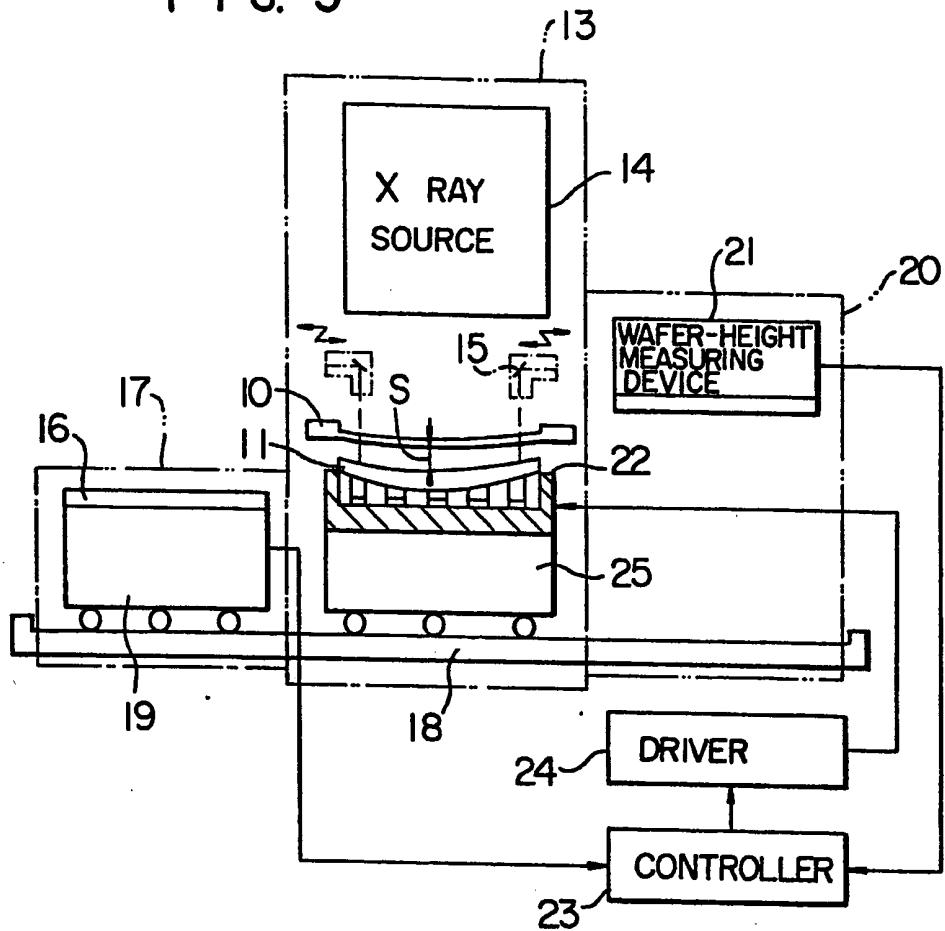


FIG. 6b

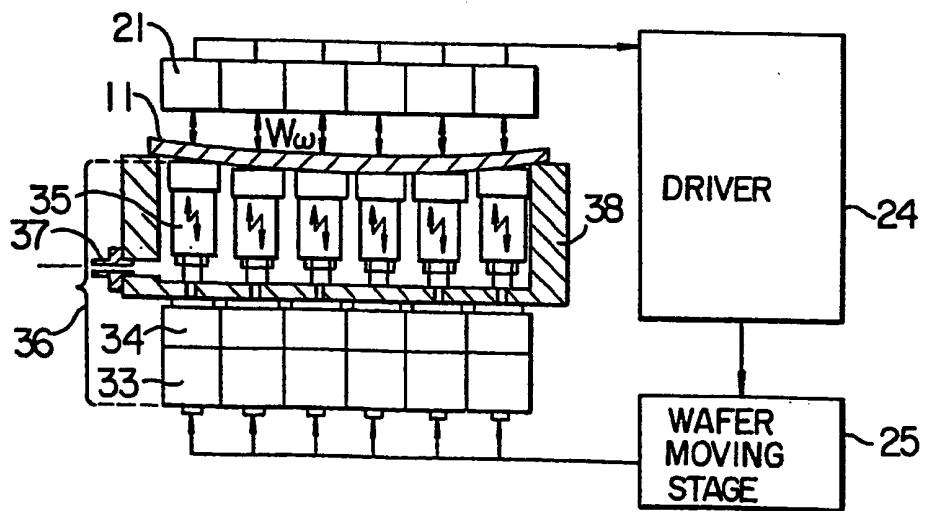


FIG. 7a

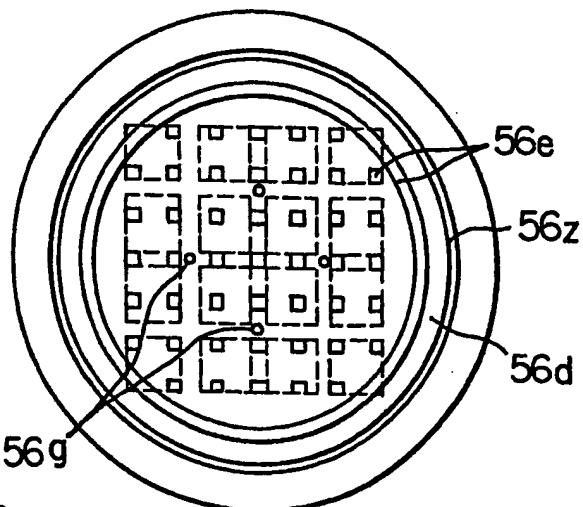


FIG. 7b

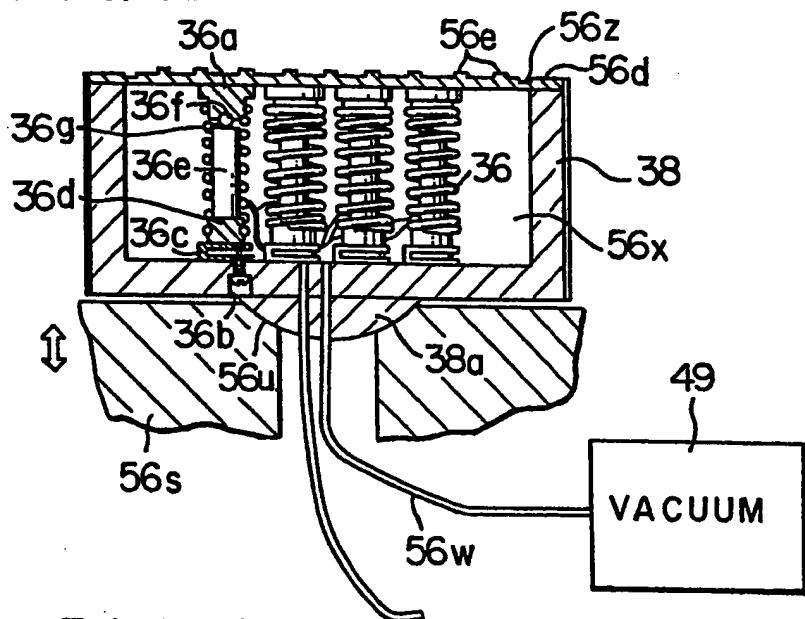
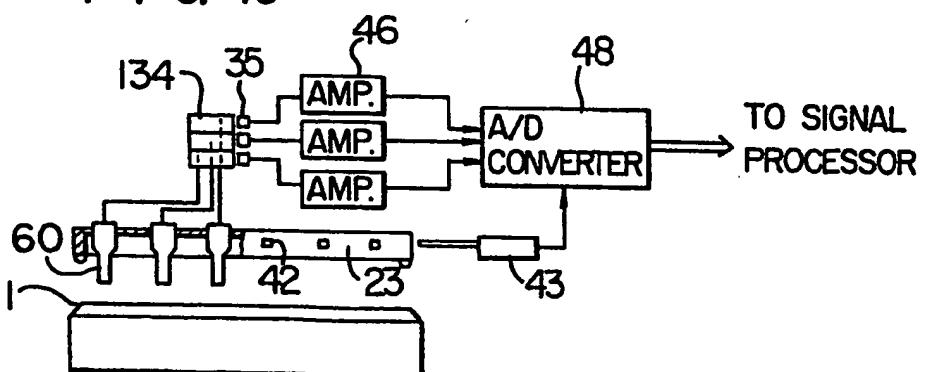


FIG. 10



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FIG. 8

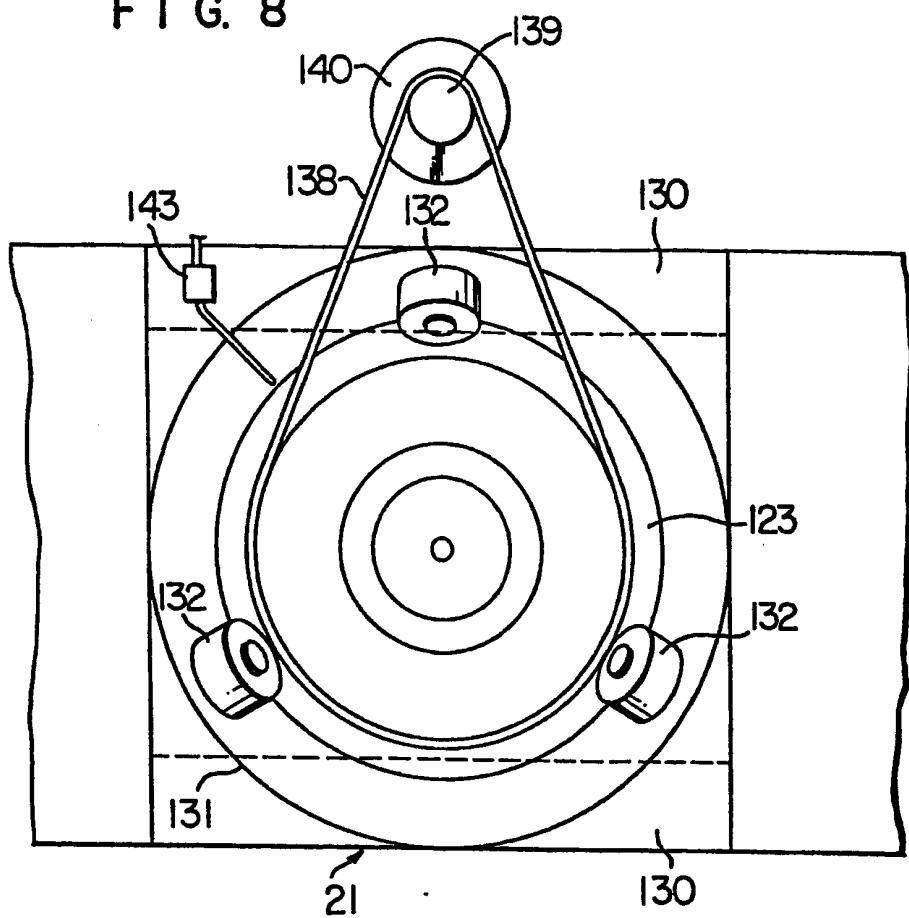


FIG. 9

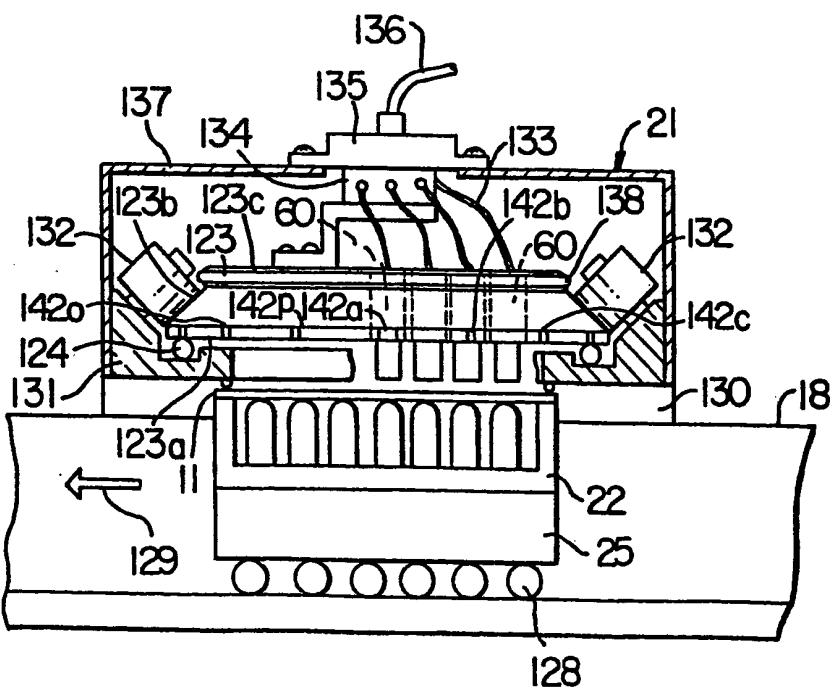


FIG. 11

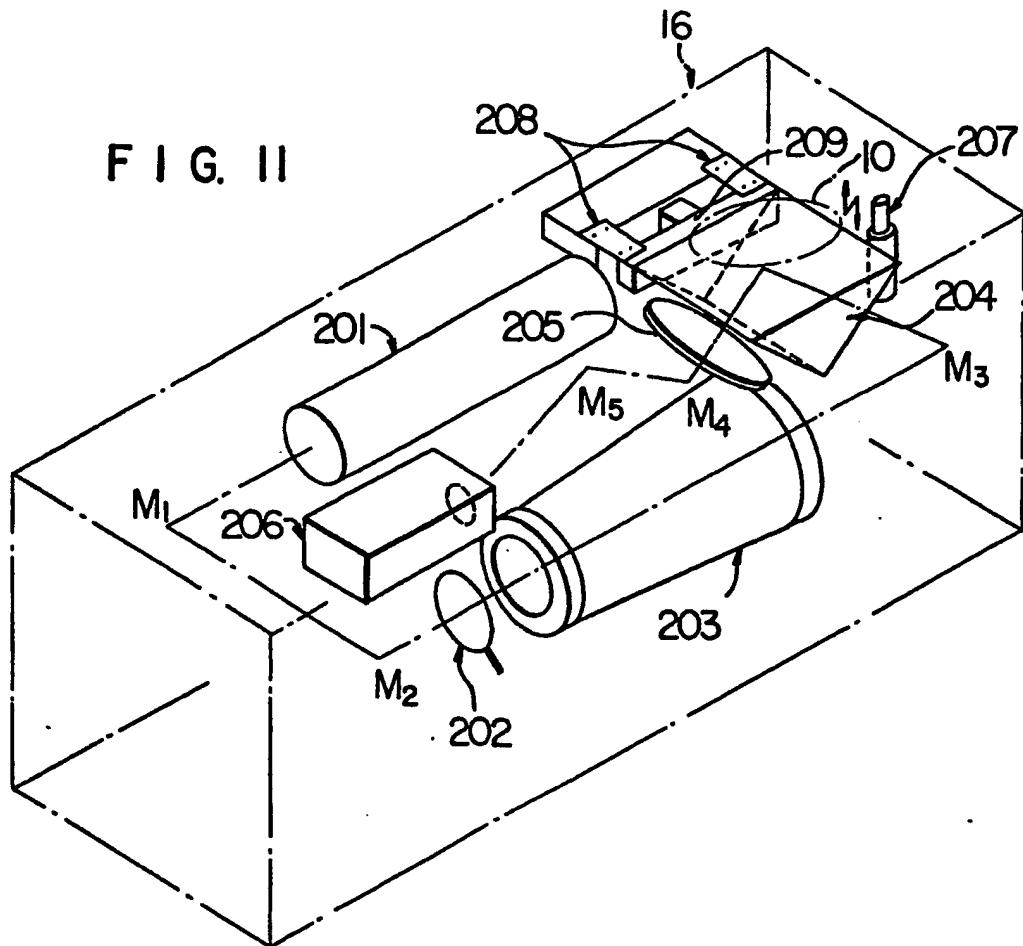


FIG. 12

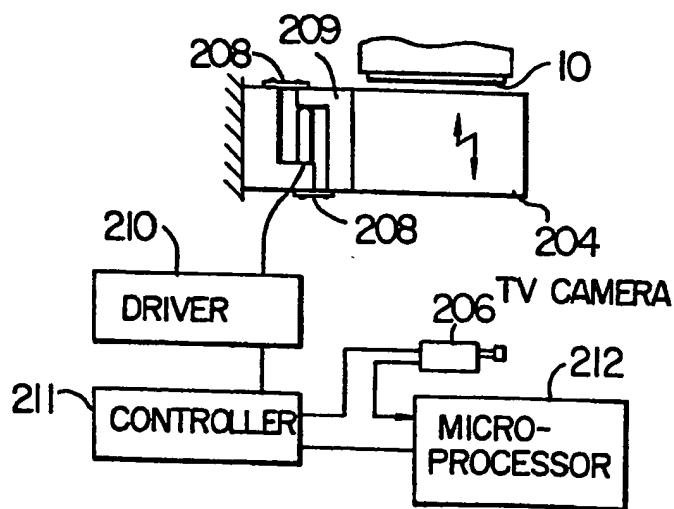
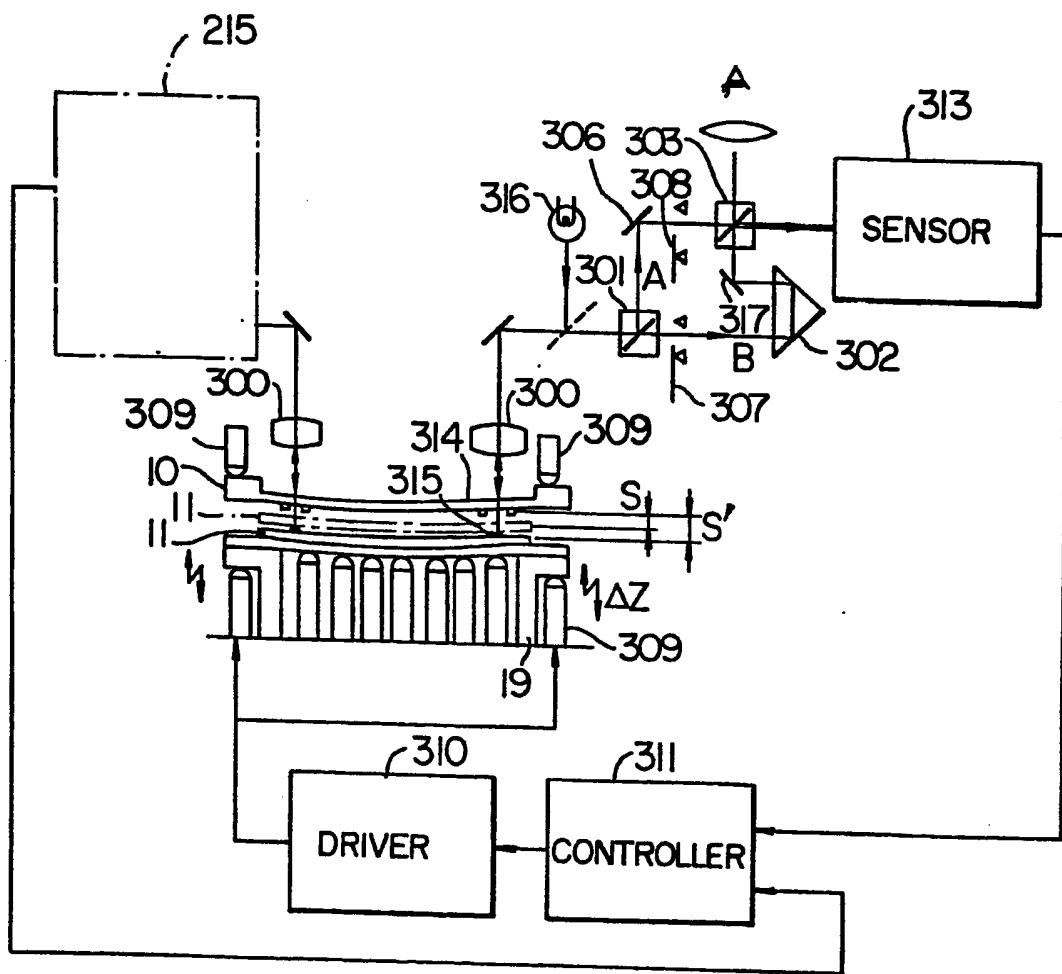


FIG. 13





DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl. 5)
Y	US-A-4 218 136 (S. KOMORIYA et al.) * column 4, lines 28-33; figure 1 * --- DE-A-2 942 388 (HITACHI LTD.) * claim 1; figure 10 * & GB - A - 2 035 610 --- EP-A-0 012 911 (INTERNATIONAL BUSINESS MACHINES CORP.) * page 4, lines 13-28 *	1,3	G 03 B 41/00
A	US-A-4 122 335 (P.A. SULLIVAN) * abstract; column 2, lines 19-24 * --- US-A-4 179 110 (M. KOGUGI et al.) * column 1, line 67 - column 2, line 8 *	1,3	
A	US-A-4 155 642 (M. LACOMBAT) * column 1, lines 25-42; column 2, lines 11-35 *	1	
A	US-E- 30 601 (A.F. HORN et al.) * column 2, lines 34-40; column 5, lines 41-49 *	1,3,5	
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		-/-	
The present search report has been drawn up for all claims			
Place of search		Date of completion of the search	Examiner
THE HAGUE		13-09-1982	PRATSCH H.R.
CATEGORY OF CITED DOCUMENTS			
X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document			
T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document			



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## EUROPEAN SEARCH REPORT

0077878

**Application number**

EP 82 10 5096

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DOCUMENTS CONSIDERED TO BE RELEVANT			Page 2
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl. *)
E, P	<p>DE-A-3 110 341 (HITACHI, LTD.)  * claims 1-16 *</p> <p>-----</p>	1-3	
			TECHNICAL FIELDS SEARCHED (Int. Cl. *)
<p>The present search report has been drawn up for all claims</p>			
Place of search	Date of completion of the search	Examiner	
THE HAGUE	13-09-1982	PRATSCH H.R.	
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P : intermediate document	& : member of the same patent family, corresponding document		



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**0 077 878**  
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⑫

## EUROPEAN PATENT SPECIFICATION

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④ Exposure process for transferring a mask pattern to a wafer.

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**25.09.85 Bulletin 85/39**

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④ References cited:  
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**DE-A-2 942 388**  
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**US-A-4 155 642**  
**US-A-4 179 110**  
**US-A-4 218 136**  
**US-E- 30 601**

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**EP 0 077 878 B1**

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### Description

The present invention relates to an X-ray exposure process and system of forming a predetermined pattern provided in a mask on such a substrate as a silicon wafer, bubble wafer, ceramic substrate or printed circuit substrate with use of X-rays.

A recent demand for highly integrated semiconductor circuit requires a finer or accurate pattern fabrication. In the state of the art, a 1 or 2  $\mu\text{m}$  pattern can be obtained by the photolithographic process, for example, by the ultraviolet ray-exposure process of reflection or reduction projection type. In order to obtain an even more integrated semiconductor circuit, a 1  $\mu\text{m}$  or less pattern, so-called submicron pattern is necessary. However, it is difficult to obtain a high-resolution projection image by the conventional photolithographic process, because the process involves undesirable problems such as optical diffraction, multi-reflection and interference. Recent researches have developed an X-ray exposure process based on soft X-rays having wavelengths between about 0.4 nm and 1.4 nm (4 and 14  $\text{\AA}$ ) in order to eliminate the above problems.

Explanation will first be directed to the principle of the known X-ray exposure process with reference to Fig. 1.

In operation, when electron beams 4 emitted from an electron gun 3 are accelerated and directed to a target 5 within a vacuum chamber 2 which is kept therein at a high vacuum level (below  $10^{-4}$  Pa), characteristic X-rays 6 depending upon the material of the target are radiated from the target 5. The X-rays 6 are emitted from the chamber 2 through a window 7 mounted thereon. The window 7 can pass or transmit, for example, beryllium(Be) X-rays alone. The rays 6 are then projected from the window 7 via a mask 10 onto a resist 12 which is coated on a wafer 11 and reacts with the X-rays 6. After exposed to the X-rays 6, the resist 12 on the wafer 11 is developed to thereby transfer a pattern 9 onto the wafer 11. The mask 10 comprises a mask carrier or base 8 made of a material (for example,  $\text{SiO}_2$ ,  $\text{Al}_2\text{O}_3$  or the like) permeable to X-rays, and the pattern 9 carried on the carrier 8 and made of an X-ray absorbing metal such as gold. In this system, the use of soft X-rays with short (4 to 14  $\text{\AA}$ ) wavelengths causes less diffraction and scattering due to dusts on the wafer 11, allowing a highly accurate transfer of the fine or complicated pattern on the wafer.

Since it is practically difficult to obtain a flux of parallel X-rays in the X-ray exposure system, X-ray flux radiated from the target 5 is usually used. For this reason, the pattern 9 on the mask 10 is transferred on the wafer 11 in a distance "b"-offset positional relationship. The pattern offset amount "b" is given as

$$b = \frac{W}{2D}$$

where D denotes a distance from the electron beam gun 5, S denotes a gap between the mask 10 and the wafer 11, and W denotes an effective mask diameter (dimension between the outermost ends of the pattern). Further, since the X-rays 6 are emitted from the target 5 corresponding to the spot diameter "d" of the electron beams, the pattern 9 on the mask 10 is transferred on the wafer 11 with an out-of-focus or defocus amount C. The out-of-focus quantity C is geometrically calculated as

$$C = \frac{d}{D}$$

In order to transfer a very fine (submicrometer) pattern on a wafer with use of the X-ray exposure system, the out-of-focus amount C must be adjusted below 0.1  $\mu\text{m}$ . On the other hand, the absolute value of the pattern offset "b" does not provide effect directly on the transfer accuracy, but variations in the offset "b" from one lithograph to another must be in the range of  $\pm 0.1 \mu\text{m}$ . If the spot diameter "d" of the electron beams 4 is 3 mm, the distance D from the X-ray source 5 to the mask 10 is 300 mm, the effective mask diameter W is 75 mm and the permissible out-of-focus amount C of the pattern 9 is 0.1  $\mu\text{m}$ , then the gap S between the mask 10 and the wafer 11 is 10  $\mu\text{m}$ . In order to make  $\pm 0.1 \mu\text{m}$  variations in the pattern offset "b", variations in the gap S must be in the range of  $\pm 0.8 \mu\text{m}$  (about  $\pm 1 \mu\text{m}$ ).

The X-ray exposure system so far suggested at its experiment and research level, has a difficulty that, as shown in Fig. 2, the gap S between the mask 10 and the wafer 11 is not constant, because the thin and weak mask 10 tends to deform or distort highly, which makes it difficult to transfer the pattern with high accuracy.

More specifically, in the suggested X-ray exposure system, the mask carrier or base 8 is made of material permeable to the X-rays 6, for example, macromolecular material such as  $\text{SiO}_2$ ,  $\text{Al}_2\text{O}_3$  and polyimide, and is of thin film having a thickness of several microns to several tens microns. Therefore, the mask 10 is weak in strength and tends to deform under varying environmental pressure and temperature. And this tendency of the mask 10 becomes remarkable as the mask is made larger, which has, so far, hindered the development of an X-ray exposure system on a batch basis.

On the other hand, the wafer 11 has a thickness of about 200 microns and thus is relatively thick and less in deformation and distortion, when compared with the mask 10. While, the wafer 11 has a evenness or flatness of usually above 4 microns and sometimes  $\pm 10 \mu\text{m}$ . However, it is practically difficult to enhance the flatness of the wafer 11 in the current-level wafer production process.

As has been explained above, the conventional system has a difficulty that the submicrometer pattern can not be transferred onto the wafer with

high accuracy, since the gap  $S$  between the wafer 11 and mask 10 varies in the range of  $\pm$ several tens  $\mu\text{m}$  or above and since the offset "b" and out-of-focus  $C$  of the pattern vary each time the wafer is exposed to X-rays through the mask 10.

It is an object of the present invention to provide an X-ray exposure process and system which has eliminated the above defects in the prior art, and wherein the wafer is deformed according to the mask shape so as to keep constant the gap or spacing between the wafer and mask and under this condition, the mask pattern is X-ray transferred on the wafer, thereby enhancing the yield in production of semiconductor, magnetic bubble, thick or thin film circuit or printed circuit substrate.

In order to accomplish the above object, according to the present invention, a pattern exposure station and a wafer-height measuring station are separately provided so as to allow a mask-height measuring device placed on a movable stage to measure heights on the mask surface at many points at the exposure station and also to allow a wafer-height measuring device to measure heights on the wafer surface at many points at the wafer-height measuring station, whereby the wafer is deformed according to the measured results by means of a wafer deforming mechanism so that the gap between the mask and wafer is constant or uniform when the mask is placed on the wafer. The wafer deforming mechanism functions to finely move or displace the wafer upward or downward by means of a chuck which sucks and holds the wafer at its plural points individually independently.

Next, the mask-height measuring device is moved backward from the exposure station and instead the wafer stage including the wafer deformer mechanism is moved toward the exposure station, and then the wafer is exposed to X-rays through the mask to thereby transfer a predetermined pattern on the wafer.

The X-ray exposure system according to the present invention is characterized in that a chuck comprises a plurality of displacement generating means for independently finely moving the wafer upward or downward at plural positions thereon and means for sucking and holding the wafer on the upper surface of said displacement generating means, and that the wafer is deformed according to the mask shape so as to maintain the spacing between the mask and wafer at a desired value and thereby to transfer the mask pattern on the wafer by exposing the wafer to X-rays.

The above and other objects and advantages of the present invention will become clear from the following description with reference to the accompanying drawings, in which:

Fig. 1 is a diagram showing the principle of the X-ray exposure process;

Fig. 2 is a diagram showing a gap relationship between a mask and a wafer used in a prior art system;

Fig. 3 is a diagram showing a gap relationship

between a mask and a wafer used in the present invention;

Figs. 4 and 5 are diagrams showing an X-ray exposure process and system in accordance with the invention;

Fig. 6a is a plan view of an embodiment of a wafer deforming device in accordance with the invention;

Fig. 6b is a cross-sectional view of the device of Fig. 6a;

Fig. 7a is a plan view of another embodiment of the wafer deforming device in accordance with the invention;

Fig. 7b is a cross-sectional view of the device of Fig. 7a;

Fig. 8 is a plan view of an embodiment of a wafer-height measuring device in accordance with the invention;

Fig. 9 is a front view of the device of Fig. 8;

Fig. 10 is a schematic diagram of the signal processing circuit of device of Fig. 8;

Fig. 11 is a perspective view of an embodiment of a mask-height measuring device in accordance with the invention;

Fig. 12 is a schematic arrangement of the device of Fig. 11; and

Fig. 13 is a detailed arrangement of an alignment scope used to measure a gap between the mask and wafer at a alignment target mark position.

An X-ray exposure process and system according to the present invention will be detailed. The principle of the X-ray exposure process is as shown in Fig. 1. As has been explained earlier in connection with the prior-art X-ray exposure process, it is difficult, in the prior art, to maintain constant the gap  $S$  between the mask 10 and wafer 11 as shown in Fig. 2, since the mask 10 tends to deform or warp and the thickness tolerance of the wafer 11 varies. A major feature of the present invention is to deform the wafer 11 according to the shape of the mask 10 to thereby make constant the gap  $S$  between the wafer and mask, as illustrated in Fig. 3.

There is shown an embodiment of the X-ray exposure process according to the invention in Figs. 4 and 5 wherein the mask 10 and a position detector or alignment scope 15 (which will be described later) for aligning the wafer 11 with the mask 10 are provided below an X-ray source 14 in the X-ray exposure station 13.

More specifically, the electron gun 3 and the target 5 are as an X-ray generating source placed within the vacuum chamber 2 which is kept therein at a high vacuum level (below  $10^{-4}$  Pa). On the vacuum chamber 2 near the target 5 is mounted the window 7 through which the X-rays 6 are emitted from the chamber 2 into another atmosphere (He atmosphere) 50.

In a practical system, generally, the target 5 is of water-cooled and rotary type in order to obtain strong X-rays. Further, the target 5 is often made of metal such as Al, Si or Pd. In this case, the radiated X-rays have wavelengths between 0.8 nm and 0.4 nm (8 and 4 Å).

The window 7 must be able to bear or withstand a pressure difference of about 100 kPa between the vacuum chamber 2 and a He chamber 51, and at the same time must be made of material permeable to X-rays. The window 7 may be approximately between 2 and 3 cm<sup>2</sup> in its area and may be of thin Be film of 25 microns or less in thickness so long as the window is disposed near the target 5, which is enough to withstand the pressure difference between the chambers.

Since such a thin film can be used for the window 7, this can also reduce the attenuation factor of the X-ray. The X-rays 6 passed through the window 7 are directed to the wafer 11 via the pattern of the mask 10 which is attached directly to the lower end of the He chamber 51. The chamber 51 is filled with a He gas, etc. and kept at an atmospheric pressure (100 kPa). The mask 10 is deformable and has a thickness of several  $\mu\text{m}$ . The mask also comprises a carrier or base 8 made of  $\text{SiO}_2$ ,  $\text{Al}_2\text{O}_3$  and the like permeable to X-ray and a circuit pattern 9 made of such X-ray absorbent material as gold. The mask is removably attached to the lower end of the chamber 51 with the mask engaged with a mask holder 52.

In order to allow an X-ray transfer of a lot of wafers 11 with use of a single piece of mask 10 and correspondingly raise its throughput remarkably, the mask 10 must be aligned accurately with the pattern of wafer 11 with the mask mounted on the lower end of the chamber 51. For this purpose, the wafer 11 is fixed on a wafer table 25 in a relation to a very-small-spacing S spaced from the mask 10. When the wafer 11 is spaced such a small gap from the mask 10, the X-ray attenuation is 0.1% and thus can be neglected.

The alignment scope 15 is disposed to allow its horizontal movement and achieve alignment between the mask 10 and wafer 11. Alternatively, since the alignment scope 15 containing therein optical and image elements (linear image sensors) and/or image devices and the like may be sealed, a portion of the scope 15 may be disposed outside of the chamber 51, if necessary. The wafer 11 is comprised of a wafer substrate coated thereon with resist. In order to achieve a proper alignment between the wafer 11 and mask 10, a wafer stage 25' is provided in the wafer table 25 to allow X, Y, Q and Z direction movements for fine or coarse adjustment. Reference numeral 53 is a diaphragm.

On the other hand, a mask-height measuring device 16 is built in the stage 19 to allow movement from the X-ray emitting station 13 to a standby position 17, and functions to measure heights Wm of the mask 10 at a plurality of points in the station 13. The stage 19 in turn slidably moves along a straight guide rail 18 accurately. Also, a wafer-height measuring station 20 is provided next to the X-ray emitting station 13, and a wafer-height measuring device 21 in the station 20 is used to measure heights Ww of the wafer 11 at a plurality of points. The wafer 11 is sucked and held by a wafer deforming chuck 22. A

controller 23 calculates the gaps S between the mask and wafer on the basis of the mask heights Wm and wafer heights Ww measured at the corresponding points thereof, and instructs a wafer height compensation amount  $\Delta Ww$  to a drive controlling section 24 so that the gaps S become constant at the respective points of the mask and wafer. According to the instruction data, the drive controlling section 24 provides corresponding compensation inputs for a plurality of wafer deforming chucks 22 and deforms the wafer 11.

The wafer height compensation  $\Delta Ww$  is given as

$$\Delta Ww = (S + h) - (Wm + Ww),$$

where "h" is a height difference between the reference surfaces of the mask-height and wafer-height measuring devices and S is a set gap between the mask and wafer. However, it will be understood that the calculation procedure is different depending on the different measuring method and the different setting of the measuring references and thus does not need to always follow the above calculation equation.

The wafer deforming chuck 22 is provided on the wafer feed or movement stage 25 and thus is moved toward the X-ray exposure station 13 along the straight guide rail 18. On the other hand, as has been described in the foregoing, the mask-height measuring device 16 is moved toward the standby position 17 by the stage 19 which carries the device 16, after measuring the mask height. Fig. 5 shows the state when the X-ray exposure process and system of the invention shown in Fig. 4 is in its X-ray exposure mode.

The wafer movement stage 25 which moves the wafer 11 into the X-ray exposure station 13, also contains therein the Y, Q and Z movement mechanism 25' as a wafer-position adjusting mechanism for position alignment between the wafer 11 and the mask pattern. The alignment scope 15 is moved and positioned above the mask 10 before X-ray exposure. After aligned with the wafer movement stage 25 for pattern alignment, the scope 15 is moved up to the standby position to avoid the blockage of X-ray passage by the scope and allow the proper exposure of the wafer to X-rays.

On the other hand, the wafer 11 can be deformed in the following two manners. That is, the heights of the mask 10 and wafer 11 are measured and according to the measured results, the wafer 11 is deformed at the wafer-height measuring station 20. The measured mask and wafer heights are pre-stored and according to the stored data, the wafer 11 is deformed at the X-ray exposure station 13. These two manners can be selected according to the system's controlling requirements.

Next, the wafer deforming procedure and the structure of the wafer deforming chuck 22 will be explained with reference to an embodiment of the present invention.

Figs. 6a and 6b show an embodiment of the wafer deforming chucks wherein the wafer 11 is conformed to the shape of the mask 10 by moving upward or downward up/down elements in the chuck and deforming the wafer. Figs. 6a and 6b are a plane view and cross-sectional view, respectively, of the detailed structure of the wafer deforming device. For one of the gratings divided as shown in Fig. 6a, an up/down displacement unit 36 is provided which comprises a motor 33, a gear 34, and an up/down element 35 having feed screw, as shown in Fig. 6b. The wafer deforming chuck device shown in Figs. 6a and 6b has the separately driven up/down displacement units 36, the wafer-height measuring units 21 provided for the respective displacement units 36, a chuck body 38 contained therein with the displacement units 36 for sucking and holding the wafer 11, a piping 37 communicated with a vacuum piping (not shown) for putting the inside of the chuck body under vacuum, the controller 23 used to calculate all the measured wafer-height and mask-height values and determine the up/down amount  $\Delta W_w$  for each of the up/down displacers 36, and the drive controlling section or driver 24 for driving the motors 33.

The wafer 11 is vacuum attracted in such a manner that the wafer follows or conforms to the tip ends of the up/down displacement units 36, and thus the wafer surface can be moved or displaced upward or downward locally by selectively actuating the respective units 36.

After the measurement of the wafer-height and mask-height, the motors 33 rotate respectively by amounts corresponding to respective correction  $\Delta W_w$  to thereby move upward or downward the up/down elements or feed screws 35 via the reduction gears 34 through which the rotational movement of the motor is reduced. In the case where a DC motor is used as the motor 33, the reduction ratio of reduction gear 34 must be as large as 10,000:1 to 100,000:1. On the other hand, when a pulse motor is used as the motor 33, the gear reduction ratio can be small enough to be able to control the up/down element 35 for every approximately 0.5  $\mu\text{m}$  increments or decrements, without any need for such a large gear ratio as in the case of DC motor. Further, the use of the DC motor facilitates an up/down amount control by the detector 21 in a closed loop, whereas the use of the pulse motor allows an open loop control. The DC motor is disadvantageously larger in size and provides more heat even during its stoppage than the pulse motor. In either case of the DC and pulse motors, backlash or play must be eliminated or suppressed to a controllable or permissible level.

In short, the wafer deforming chuck 22 has a plurality of up/down elements 35 at its upper side and the elements 35 can be separately displaced upward or downward by the respective up/down displacement units 36 to allow fine adjustment.

Also, the displacement units 36 may be replaced not only by the above-mentioned screws coupled to the motors but also by piezoelectric

elements, magnetostrictive elements, thermally deforming elements, magnet- or fluid-based units, fine displacement mechanism based on lever, or combination thereof. In the case of semiconductor wafer, the stroke of the displacement unit 36 must be 30  $\mu\text{m}$ , the positioning accuracy must be below  $\pm 1$  micron, the deformation rate must be faster than the throughput rate, and the wafer must be stable during its X-ray exposure.

As disclosed in Fig. 7 in USP Serial No. 245,193 filed in March 18, 1981, a thin film 56d may be applied over the displacing devices 36. A structure of the thin film 56d will be described later. The displacing device 36 may comprise a member 36a bonded to the bottom surface of the thin film 56d, a U-shaped member 36c which is clamped to the chuck body 38 and can be level-adjusted by a screw 36d, a member 36d clamped to the member 36c, a piezoelectric element 36e having its lower end fixed to the member 36d, a ball 36f disposed between the upper end of the piezoelectric element 36e and the lower end of the member 36a and a spring 36g for tensioning the member 36a and the member 36d. A sphere 38a is mounted on the bottom surface of the chuck body 38. A stage 56s which supports the sphere 38a of the chuck body 38 by a spherical seat 56u is movable upward and downward by a lead screw mechanism, not shown. Since the substrate 11 is deformed through the thin film 56d while the substrate 11 is sucked and held by the thin film 56d, no localized stress is applied to the substrate 11 and the breaking of the substrate is prevented and the exposure surface of the substrate 11 can be smoothly deformed to conform to a desired shape.

In an alternative of the displacing device 36, vacuum pressures to a plurality of chambers may be adjusted to deform the thin film 56d in the shape of diaphragm. Numeral 56g shows a bore through which the substrate 11 is sucked to the thin film 56d.

The substrate deformation measuring device 21 may be of contact type or non-contact type. The contact type includes a dial gauge device and the non-contact type includes an air micrometer, electromagnetic device, static capacitance device and optical device. The substrate deformation correcting thin film 56d is made of a thin, flexible metal plate such as steel, aluminum, stainless steel, phosphor bronze or silicon, having a thickness of 0.4–3 mm, a thin glass plate having a thickness of approximately 0.7 mm, or a thin resin plate such as Tefuron. It has ring-shaped ribs 56e of approximately 50–100  $\mu\text{m}$  height around an outer periphery thereof and regularly arranged within the outer periphery. A chuck body 38 having a flexible wafer chuck surface 56d integrally fixed to the upper end of a cylinder 56b is mounted inside the rib 56e. The rib 56 may be of square shape or circular shape. In order to support the periphery of the wafer chuck surface 56d substantially freely, a ring-shaped groove 56z is formed to reduce the thickness. In order to eject

the exposed wafer 11 by an air jet force, an obliquely oriented transport hole 56g is formed. The hole 56g is connected to a room 56x formed in the chuck body 38. The path 56x is connected to a vacuum source 49 through a flexible pipe 56w.

The wafer-height and mask-height measuring devices are each classified into contact type and non-contact type. A typical example of the contact type measuring devices is a dial gauge, but it is not suitable for mask-height measurement applications because the mask 10 is thin and tends to easily deform. On the other hand, the non-contact type measuring devices include, for example, an air micrometer, an electromagnetic instrument, an electrostatic capacity type instrument, an optical instrument, an ultrasonic-wave based instrument.

An example most preferable as the wafer-height measuring device 21 is disclosed in USP Serial No. 292,933 (filed in August 14, 1981) herein as Figs. 8 to 10. The example will be explained below with reference to Figs. 8 to 10. Referring now to Fig. 9, the wafer deforming chuck 22 mounted on the wafer feed stage 25 is supported slidably in an arrowed direction 129 by air bearings 128 rested on the straight guide rail 18. The deformation amount of the wafer 11 surface is detected and stored at the wafer-height measuring station 20.

As illustrated in Fig. 9, a disc 123 is disposed in parallel with the wafer 11. The disc 123 is carried on the straight guide rail 18 through air bearing 128. The upper surface of the straight guide rail 18 and the lower surface 123a of the disc 123, contacting with the steel balls 124, are carefully and precisely flattened. The base 131, circular in shape, is fixed on. Accordingly, the disc 123 continues its rotation in a fixed direction, being precisely kept parallel to the wafer 11, by means of the combination of the base 131, the steel balls 124 and the rotating bearings 132.

The disc 123 is provided with a plurality of detecting probes 60 directed at their tips toward the surface of the wafer 11 for detecting distances from the tips thereof to the surface of the wafer 11.

The plurality of detecting probes 60 mounted to the disc 123 are arranged in a linear or curved fashion from the center of the disc 123 to the peripheral portion thereof.

The detecting signals from the detecting probes 60 are led out through cables 133. The cables 133 are fixed to a rotating side 134 of a slip ring which is held by the disc 123 and moves together with the disc 123. The detecting signals further travel from a stationary side 135 of the slip ring which is held by a holder frame 137 fixed to the spacers 130, through a cable 136, to a signal processing means containing a display, an arithmetic unit, a CRT and the like. The signal from the cable 136 is an analog signal produced through one revolution of the disc 123. For the signal processing, the analog signal may directly be used for representing the flatness information of the wafer 11. Alternatively, the analog signal may be converted,

every given rotational angle of the disc 123, into a digital signal which is used as the flatness information of the wafer 11. In any case of using a digital or analog signal, it is desirable to provide means for detecting rotation position of the disc 123. The disc 123 in Fig. 9 is additionally provided with means for detecting timings to perform the A/D conversion, that is to say, for finding measuring locations on the wafer 11, i.e. rotation position of the disc 123. To be more specific, a plurality of marks 142a, 142b, ... are stucked around the lower portion of the shoulder 123b of the disc 123, being arranged equidistantly. When the A/D conversion is performed every 1/16 revolution of the disc 123, sixteen marks 142a, 142b, ... 142p are stucked to the lower shoulder portion every rotation of 22.5°. In this case, the passage of the mark is sensed by a photosensor 143 shown in Fig. 8 and an output signal from the photosensor is used as a timing signal for the A/D conversion or the measuring position data for the wafer 11. If one of the sixteen marks is longer than the remaining ones, a signal representing a rotation start or an origin of the timing signal can be obtained from the longer mark.

Circuit diagram for processing output signals from the detecting probes 60 in synchronism with timing signal obtained by the photosensor 143 to obtain the degree of flatness of the wafer 11 will be explained referring to Fig. 10. Fig. 10 shows an example in which three electrostatic capacitor type sensors are used as the detecting probes 60. In Fig. 10, reference numeral 46 shows current-voltage converting amplifiers each for converting output current from the corresponding detecting probe 60 into a current signal, and 148 shows an analog-digital converter for converting analog voltage signals from the amplifiers 46 into digital signals in response to a timing signal from the photosensor 143. The digital output signal of the A/D converter 148 is applied to a signal processor including a CPU (not shown) for calculating degree of flatness of the wafer 11.

In this way, the deformation amounts on the wafer 11 surface at many points are detected at the wafer-height measuring station 20. The detecting probe 60 may be such an electrostatic capacity sensor as disclosed in USP Application No. 64240. The deformation amounts on the wafer 11 surface can be detected by the sensor because the wafer 11 is grounded.

Detailed explanation will next be directed to how the mask-height measuring device 16 detects the deformation amounts on the easy-to-deform mask 10. Fig. 11 shows an arrangement or structure of the mask-height measuring device 16. In the figure, He-Ne laser rays emitted from a laser tube 201 are guided via reflection mirrors  $M_1$  and  $M_2$  to a deflection plate 202 the rotation of which acts to change the intensity of the received laser rays. The laser rays intensity-adjusted at the deflection plate 202 are then entered in a beam expander 203 to form a laser beam having a spot diameter or size of 30 mm on the mask 10. The laser beam exiting from the expander 203 is

directed via a reflection mirror  $M_3$  into a prism 204. Interference fringe of equal thickness appeared on the prism surface and the mask surface is imaged on the tube of a TV camera 206 through an imaging or focusing lens 205. Reference numerals  $M_4$  and  $M_5$  are also reflection mirrors. An electrostatic capacity sensor 207 is provided next to the prism 204 to detect the absolute value of the height corresponding to a point on partial conductive thin film formed in the periphery of the mask 10.

The prism 204 is supported by a spring set or leaf springs 208 to allow a fine up/down displacement. More particularly, the prism can be finely moved upward or downward by a piezo-electric element 209 having a maximum stroke of 25  $\mu\text{m}$ , as shown in Fig. 12.

Fig. 11 shows the basic principle of how the interference fringe of equal thickness are developed or generated. The deformation amounts on the mask surface appear in the form of contour lines in the interference bands, since the parallel laser rays in phase are interfered with their components reflected at the prism surface and their components reflected at the mask surface. The difference of distance between surfaces of the prism and the mask corresponding to positions at which contour lines in the interference bands exist is determined by the angle of incidence when the laser rays enter into the mask surface and the wavelength of the laser beam. The distance can vary from about 0.3  $\mu\text{m}$  to infinity ( $\infty$ ) in accordance with the change of the angle of incidence but is preferably 2  $\mu\text{m}$ . In Fig. 12, a fine displacement or movement of the prism 204 upward or downward will cause a movement of the interference bands. Therefore, the prism 204 is moved stepwise every 0.125  $\mu\text{m}$  through a driver 210 which is actuated by a command from a controller 211, and the interference band image is entered into the TV camera 206. At the same time, the position of the prism and the position of the interference band are stored in a memory in a microprocessor 212. This procedure is repeated at 16 times by an amount corresponding to the interference band pitch 2  $\mu\text{m}$ . The deformation amounts on the mask 10 can be found by analyzing or calculating the positions of the prism and the positions of the interference band corresponding to 16 times with use of the microprocessor 212. That is to say, in case the surface of the mask projects in the down direction, the interference fringe is moved in the radial direction when the prism 204 is moved upward. In case the surface of the prism is concave, the interference fringe is moved in the direction of the center thereof. Therefore, the projection and the concavity of the mask can be distinguished by analyzing the movement direction of the interference fringe by the microprocessor. Moreover, when the prism 204 is moved by 0.125  $\mu\text{m}$ , difference between the height of the mask surface corresponding to position at which an interference fringe exist before the movement of the prism and that after the movement of the prism

corresponds to 0.125  $\mu\text{m}$ . Accordingly, the deformation of the mask can be measured with the precision of 0.125  $\mu\text{m}$ . The fundamental concept is known and is carried out in such a manner as disclosed in the SPIE, Vol. 135, pages 104 to 110, entitled "The Interferometric Analysis of Flatness by Eye and Computer".

On the other hand, the mask deformation amounts obtained from the prism are relative difference but the absolute height values corresponding to the deformation amounts are unknown.

For this purpose of knowing the absolute heights, the electrostatic capacity sensor 207 is used to measure the absolute values  $W_{\text{mA}}$  of heights of the conductive thin film (for example Au) in the periphery of the mask carrier or base 8 in which the LSI circuit pattern does not exist.

The absolute mask deformation value  $W_m$  is expressed as the following equation

$$W_m = F(x, y) + \Delta \quad (1)$$

where,  $\Delta$  is a constant necessary for a relative value  $F(x, y)$ . The absolute value  $F(x_0, y_0)$  at a point  $(x_0, y_0)$  measured by the sensor 207 is known with use of the prism,  $\Delta$  satisfies the following equation (2).

$$\Delta = W_{\text{mA}} - F(x_0, y_0) \quad (2)$$

In this way, the absolute deformation amount  $W_m$  on the entire mask 10 can be obtained from equation (1).

Although there has been explained in the foregoing a system wherein the absolute values of heights of the mask 10 are measured by the sensor 207 shown in Fig. 11 and the absolute values of gaps between the wafer 11 and the mask 10 are adjusted to their desired levels, an alternative system may be used. That is, the deformation amounts of the mask 10 and wafer 11 are detected by the mask-height and wafer-height measuring devices 17 and 21 based on light interference bands, and subsequently the wafer 11 is deformed by means of the wafer deforming chuck 19 so that the wafer conforms in shape to the mask 10. In this way, the wafer 11 has been deformed so as to conform to the mask 10 in shape. And by aligning alignment marks 314 of the wafer 11 with alignment marks 315 of the mask 10 with use of the optical double-focus alignment system of Fig. 13, the gap between the mask 10 and wafer 11 can be adjusted to a predetermined value  $S$ .

More specifically, the mask alignment marks 314 information is sent via an optical path A on the mask side (including an object lens 300, a beam splitter 301, a rectangular prism 302 and a beam splitter 303) to a linear image sensor 313 where the marks 314 in the information are detected. By tilting the entire mask 10 with use of a piezoelectric element 308, the marks 314 are focused on the sensor 313.

On the other hand, a shorter light path B on the

wafer side (including an object lens 300, a beam splitter 301, a mirror 306 and a beam splitter 303) is provided so that when the wafer alignment mark 315 is spaced a spacing S of about 10  $\mu\text{m}$  from the mask alignment mark 314, the wafer mark 315 becomes focused on the linear image sensor 313. Therefore, the entire deforming chuck 22 is pre-adjusted so that the gap S' between the wafer 11 and mask 10 (at the mark 314 and 315 positions) is larger than the gap S. Next, the piezoelectric element 309 for wafer tilting is moved gradually upward by a piezoelectric-element driver 310. Under this condition, a controller 311 detects the maximum of the output signal supplied from the linear sensor 313. The entire deforming chuck 19 is positioned at the focused position detected by the controller. This results in that gap between the mask 10 and wafer 11 at the mark 314 and 315 positions becomes the predetermined value S. As a result, there can be corrected a very small tilt in the wafer 11 which occurs when the wafer 11 is transferred from the wafer-height measuring device to the X-ray exposure position by moving the wafer movement stage 25 mounted at its top with the wafer. In order to detect the alignment marks 314 and 315, optical shutters 307 and 308 may be provided, if desired.

According to the present invention, as has been disclosed in the foregoing, the gap between the pattern transfer mask and wafer can be made always constant or uniform with accuracy within  $\pm 1 \mu\text{m}$  even if the mask is deformed, waved or curved, by deforming the wafer so as to conform to the shape of the mask. As a result, the offset and out-of-focus (defocused) amounts b, c of the transfer pattern can be kept constant. For example, a submicrometer (below 1  $\mu\text{m}$ ) pattern can be accurately transferred onto the wafer with use of X-rays. In addition, in photolithographic process, it is possible to transfer a fine pattern at its optical resolution limit, which leads to a remarkable improvement in the yield of such integrated circuit chips as LSI.

The mask-height measuring device 16 and the movement stage 25 have been supported slidably on the same straight guide rail 18 in the above embodiments, it will be appreciated that the device and stage are carried preferably on different straight guide rails respectively because the wafer chuck 22 must be provided with a mechanism which supplies and discharges the wafer 10 in the practical applications. That is, it is desirable to support the mask-height measuring device 16 slidably on another straight guide rail which extends in a direction perpendicular to the paper plane of Fig. 4.

#### Claims

1. An exposure process for transferring a mask (10) pattern (9) on a wafer (11), characterised in that heights on the mask surface facing the wafer at many points are measured by a mask-height measuring device (16) and heights on the wafer

surface facing the mask at many points are measured by a wafer-height measuring device (21), after which the wafer is deformed by means of a chuck (35, 36, 38) which sucks and holds the wafer at many points thereon and finely moves the wafer upward or downward individually independently at said many points according to said measurements to adjust a gap (S) of uniform width between the mask and the wafer.

5 2. An exposure process as set forth in claim 1 wherein said exposure process is of X-ray exposure type.

10 3. An exposure system for transferring onto a wafer (11) a circuit pattern (9) formed on a mask (10), characterised by a chuck (35, 36, 38) provided with means (35) for sucking and holding said wafer at many points thereon and finely moving the wafer upward or downward individually independently at said many points; a stage (19) provided with said chuck and supported slidably on a platen between an exposure position (15) and a wafer-height measuring position; a wafer-height measuring device (21) disposed opposite to the wafer moved in said wafer-height measuring position by said stage for measuring heights on the wafer at said many points; and a mask-height measuring device (16) slidably supported on said platen between said exposure position and a standby position (17) and disposed opposite to the mask at the exposure position, for measuring heights on the mask surface at many points; wherein the gap (S') between the wafer and the mask is detected according to said wafer heights measured by said wafer-height measuring device and said mask heights measured by said mask-height measuring device, and wherein said fine up/down moving means (36) are actuated so that said detected gap (S') is adjusted to an uniform width (S).

15 4. An exposure system as set forth in claim 3 wherein said exposure system is of X-ray exposure type and includes an X-ray source (14) and means (1, 2, 51, 50) for preventing the attenuation of X-rays emitted from said X-ray source and for projecting the X-rays on the mask (10).

20 5. An exposure system as set forth in claim 4 wherein said mask-height measuring device (16) includes an optical mask-height measuring means.

25 6. An exposure system as set forth in claim 5 wherein said optical mask-height measuring means measures said mask heights on light interference band basis.

30 7. An exposure system as set forth in claim 6 wherein said mask-height measuring device (16) includes a sensor (313) for detecting the absolute values of positions on the mask (10) and in the periphery thereof.

35 8. An exposure system as set forth in claim 6, further including an observation or detection optical system (215) provided within a chamber for observing or imaging an alignment mark (314 or 315) on the mask and an alignment mark on the wafer and for detecting the gap (S') between the

mask (10) and wafer (11) at said alignment mark positions respectively on the mask and wafer, and means for finely moving said entire chuck (22) upward or downward in such a manner that said gap detected by said optical system becomes a predetermined value (S).

9. An exposure system as set forth in claim 8 wherein said observation or detection optical system (215) includes a double focus optical system with different light paths (A, B).

#### Patentansprüche

1. Belichtungsverfahren zum Übertragen eines Musters (9) einer Maske (10) auf ein Plättchen (11), dadurch gekennzeichnet, daß Höhen auf der dem Plättchen zugewandten Maskenoberfläche an vielen Stellen mit einer Maskenhöhen-Meßvorrichtung (16) gemessen werden und Höhen auf der der Maske zugewandten Plättchenoberfläche an vielen Stellen von einer Plättchenhöhen-Meßvorrichtung (21) gemessen werden, wonach das Plättchen mittels einer Einspannvorrichtung (35, 36, 38) verformt wird, die das Plättchen an vielen darauf befindlichen Punkten ansaugt und hält und das Plättchen an den vielen Punkten nach Maßgabe der Messungen feinfühlig individuell und unabhängig aufwärts oder abwärts bewegt unter Einstellung eines Spalts (S') gleichmäßiger Breite zwischen der Maske und dem Plättchen.

2. Belichtungsverfahren nach Anspruch 1, wobei dieses Verfahren vom Röntgenbelichtungstyp ist.

3. Belichtungseinrichtung zum Übertragen eines auf einer Maske (10) ausgebildeten Schaltungsmusters (9) auf ein Plättchen (11), gekennzeichnet durch eine Einspannvorrichtung (35, 36, 37), die eine Einheit (35) zum Ansaugen und Halten des Plättchens an vielen Stellen desselben und zum feinfühligen individuellen und unabhängigen Auf- oder Abbewegen des Plättchens an den vielen Stellen umfaßt; einen Objektisch (19), der die Einspannvorrichtung aufweist und verschiebar auf einer Platte zwischen einer Belichtungslage (15) und einer Plättchenhöhen-Meßlage gehalten ist; eine Plättchenhöhen-Meßvorrichtung (21), die gegenüber dem Plättchen, das in der Plättchenhöhen-Meßlage durch den Objektisch zur Messung von Höhen auf dem Plättchen an den vielen Punkten bewegbar ist, angeordnet ist; und eine Maskenhöhen-Meßvorrichtung (16), die auf der Platte zwischen der Belichtungslage und einer Bereitschaftslage (17) verschiebar gehalten und gegenüber der Maske in der Belichtungslage angeordnet ist, um Höhen auf der Maskenoberfläche an vielen Punkten zu messen; wobei der Spalt (S') zwischen dem Plättchen und der Maske nach Maßgabe der von der Plättchenhöhen-Meßvorrichtung gemessenen Plättchenhöhen und der von der Maskenhöhen-Meßvorrichtung gemessenen Maskenhöhen erfaßt wird und w bei die Vorrichtung (36) zum feinfühligen Auf- und Ab-

bewegen so betätigbar ist, daß der erfaßte Spalt (S') auf eine gleichmäßige Breite (S) einstellbar ist.

4. Belichtungseinrichtung nach Anspruch 3, wobei in diese vom Röntgenbelichtungstyp ist und eine Röntgenstrahlquelle (14) sowie Mittel (1, 2, 51, 50) aufweist, die die Dämpfung der von der Röntgenstrahlquelle ausgehenden Röntgenstrahlen verhindern und die Röntgenstrahlen auf die Maske (10) projizieren.

5. Belichtungseinrichtung nach Anspruch 4, wobei die Maskenhöhen-Meßvorrichtung (16) eine optische Maskenhöhen-Meßeinheit aufweist.

6. Belichtungseinrichtung nach Anspruch 5, wobei die optische Maskenhöhen-Meßeinheit die Maskenhöhen auf der Basis von Lichtinterferenzstreifen mißt.

7. Belichtungseinrichtung nach Anspruch 6, wobei die Maskenhöhen-Meßvorrichtung (16) einen Fühler (313) aufweist, der die Absolutwerte von Positionen auf der Maske (10) und am Rand derselben erfaßt.

8. Belichtungseinrichtung nach Anspruch 6, ferner umfassend eine Beobachtungs- bzw. Erfassungsoptik (215) in einer Kammer zur Beobachtung oder Abbildung einer Ausrichtungsmarkierung (314 oder 315) auf der Maske und einer Ausrichtungsmarkierung auf dem Plättchen und zur Erfassung des Spalts (S') zwischen der Maske (10) und dem Plättchen (11) an den Ausrichtungsmarkierungs-Positionen auf der Maske bzw. dem Plättchen, sowie Mittel zum feinfühligen Bewegen der gesamten Einspannvorrichtung (22) auf- bzw. abwärts in solcher Weise, daß der von der Optik erfaßte Spalt einen vorbestimmten Wert annimmt.

9. Belichtungseinrichtung nach Anspruch 8, wobei die Beobachtungs- bzw. Erfassungsoptik (215) eine doppelfokussierende Optik mit verschiedenen Strahlengängen (A, B) ist.

#### Revendications

1. Procédé d'exposition servant à transférer une structure (9) d'un masque (10) sur une pastille (11), caractérisé en ce qu'on mesure des hauteurs sur la surface du masque, tournée vers la pastille, en différents points au moyen d'un dispositif (16) de mesure de hauteurs sur le masque et qu'on mesure des hauteurs sur la surface du masque tournée vers le masque, en de nombreux points, au moyen d'un dispositif (21) de mesure de hauteurs sur la pastille, à la suite de quoi on déforme la pastille au moyen d'un mandrin (35, 36, 38), qui assure le maintien de la pastille en de nombreux points sur cette dernière et déplace finement la pastille vers le haut ou vers le bas, d'une manière individuelle indépendante, au niveau desdits nombreux points conformément auxdites mesures de manière à régler un interstice (S') de largeur uniforme entre le masque et la pastille.

2. Procédé d'exposition selon la revendication 1, selon lequel ledit procédé d'exposition est du type à exposition aux rayons X.

3. Système d'exposition pour transférer sur une pastille (11) une structure (9) d'un circuit, formée sur un masque (10), caractérisé par un mandrin (35, 36, 38) muni de moyens (37) pour aspirer et maintenir ladite pastille au niveau de nombreux points de cette dernière et à déplacer finement la pastille vers le haut ou vers le bas d'une manière individuellement indépendante au niveau desdits nombreux points, un chariot (19) muni dudit mandrin et supporté de façon à pouvoir glisser sur une platine entre une position d'exposition (15) et une position de mesure de hauteurs sur la pastille; un dispositif (21) de mesure de hauteurs sur la pastille disposé à l'opposé de la pastille amenée dans ladite position de mesure de hauteurs de la pastille au moyen dudit chariot de manière à mesurer des hauteurs sur la pastille au niveau desdits nombreux points, un dispositif (16) de mesure de hauteurs sur la pastille monté de façon à pouvoir glisser ladite platine entre ladite position d'exposition et une position d'attente (17) et situé à l'opposé du masque au niveau de la position d'exposition, pour réaliser la mesure de hauteurs à la surface du masque en de nombreux points, l'interstice (S') entre la pastille et le masque étant détecté conformément auxdites hauteurs mesurées sur la pastille par ledit dispositif de mesure de hauteurs sur la pastille et conformément auxdites hauteurs mesurées sur le masque au moyen dudit dispositif de mesure de hauteurs sur le masque, et lesdits moyens (36) de déplacement fins vers le haut/vers le bas étant actionnés de telle sorte que ledit interstice (S') détecté est réglé à une largeur uniforme (S).

4. Système d'exposition selon la revendication 3, dans lequel ledit système d'exposition est du type à exposition aux rayons X et comporte une source de rayons X (14) et des moyens (1, 2, 51,

50) servant à empêcher l'atténuation des rayons X émis par ladite source de rayons X et servant à projeter les rayons X situés sur le masque (10).

5. Système d'exposition selon la revendication

4, dans lequel ledit dispositif (16) de mesure de hauteurs sur le masque comporte des moyens optiques de mesure de hauteurs sur le masque.

6. Système d'exposition selon la revendication 5, dans lequel lesdits moyens optiques de mesure de hauteurs sur le masque mesurent lesdites hauteurs sur le masque sur la base de bandes d'interférences lumineuses.

7. Système d'exposition selon la revendication

6, dans lequel ledit dispositif (16) de mesure de hauteurs sur le masque comporte un capteur (313) servant à détecter les valeurs absolues des positions sur le masque (10) et sur la périphérie de ce dernier.

8. Système d'exposition selon la revendication

6, comportant en outre un système optique d'observation ou de détection (215) logé à l'intérieur d'une chambre pour l'observation ou la formation d'images d'une marque d'alignement (314 ou 315) sur le masque et d'une marque d'alignement sur la pastille et pour la détection de l'interstice (S') entre le masque (10) et la pastille (11) au niveau des positions desdites marques d'alignement respectivement sur le masque et sur la pastille, et des moyens pour déplacer finement l'ensemble dudit mandrin (22) vers le haut ou vers le bas de telle manière que ledit interstice détecté à l'aide dudit système optique prenne une valeur prédéterminée (S).

9. Système d'exposition selon la revendication

8, dans lequel ledit système optique d'observation ou de détection (215) comporte un système optique à deux foyers, avec des trajectoires différentes (A, B) de la lumière.

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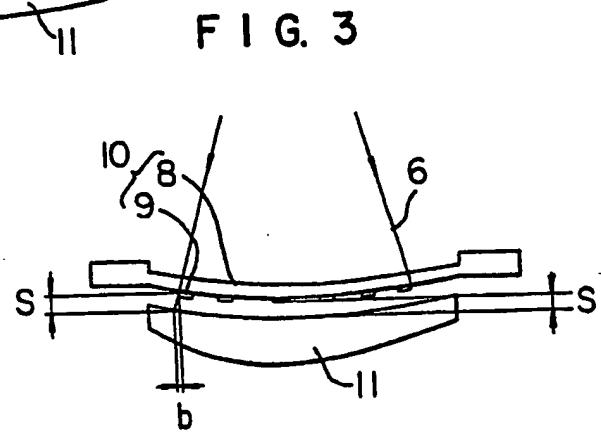
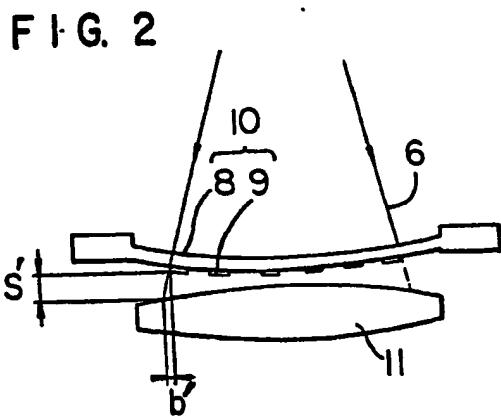
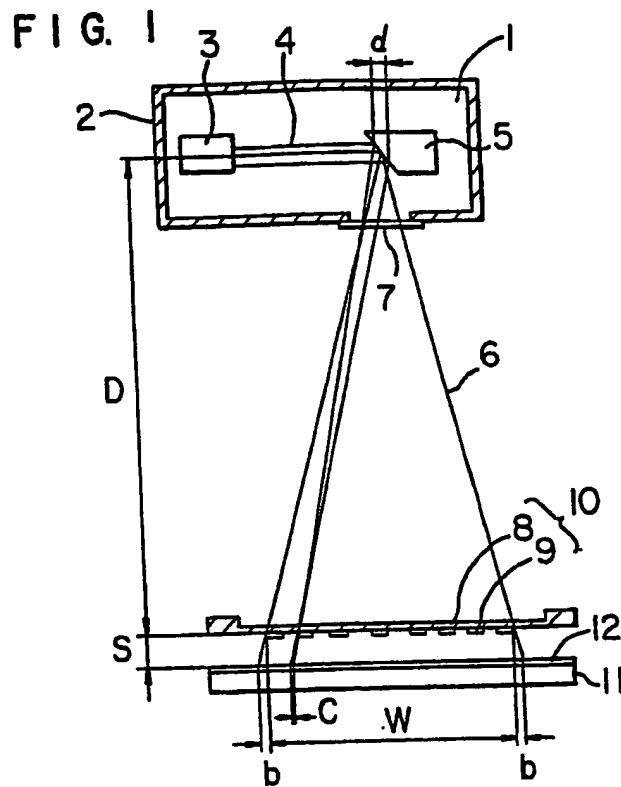


FIG. 4

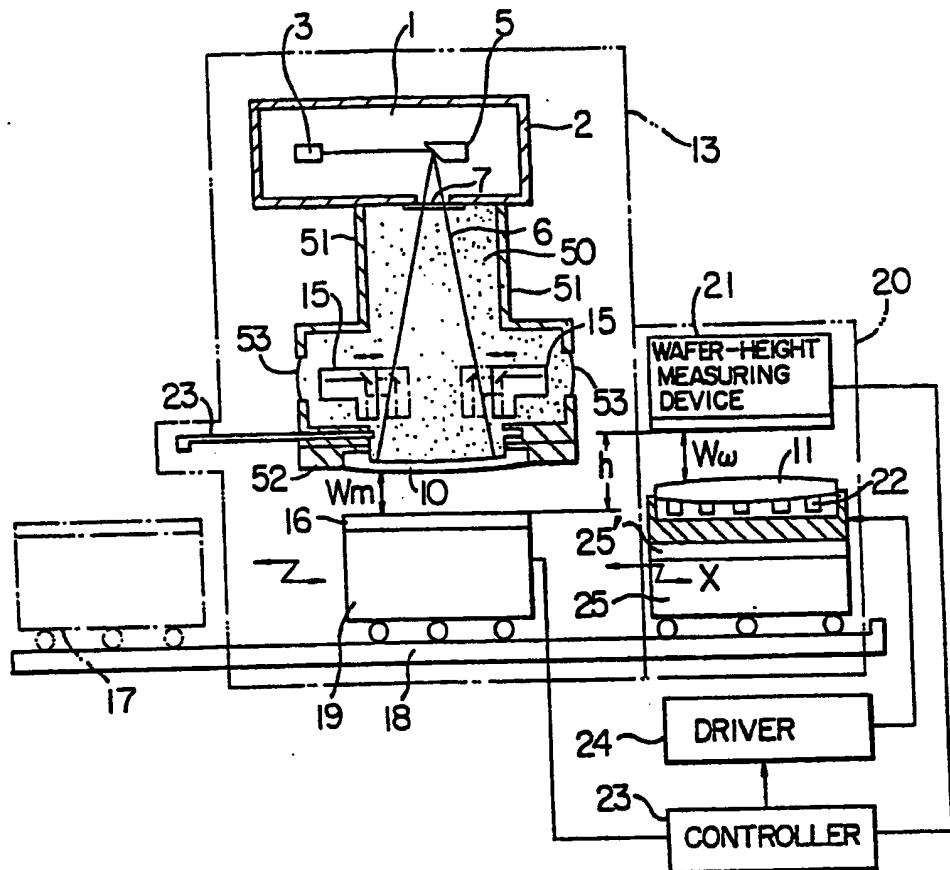
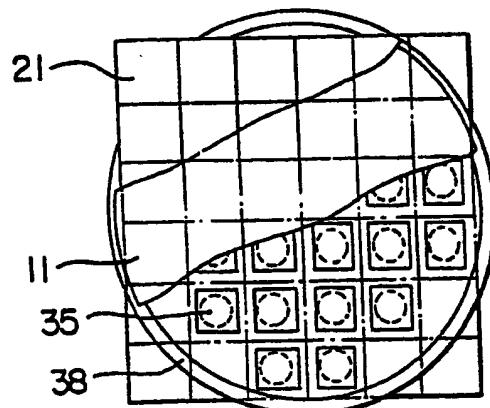
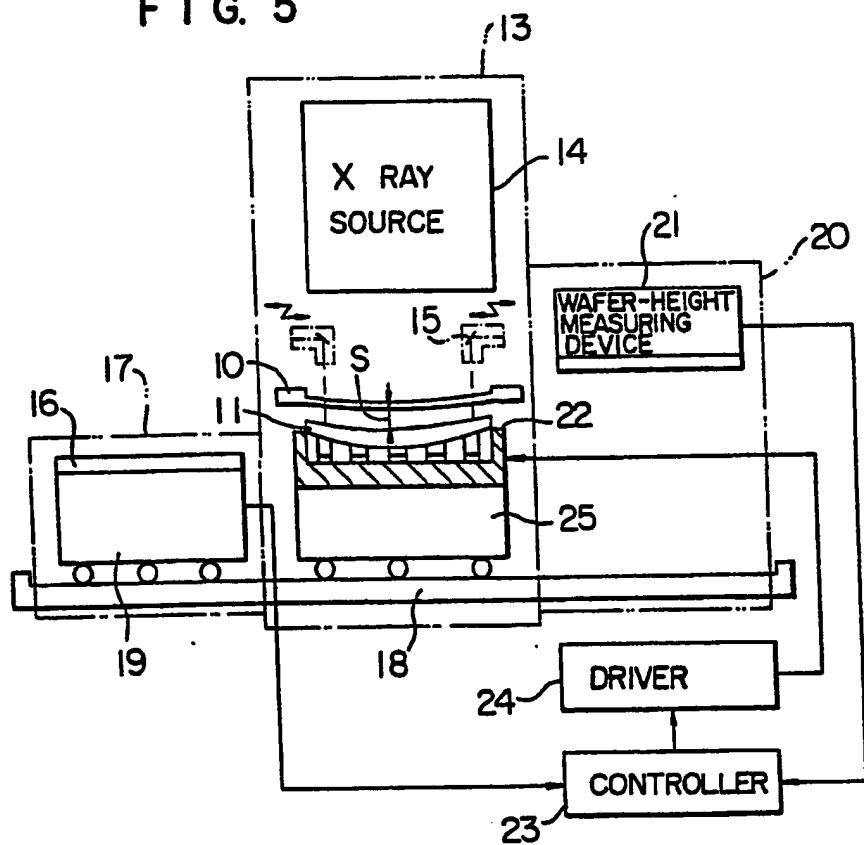


FIG. 6a



F I G. 5



F I G. 6b

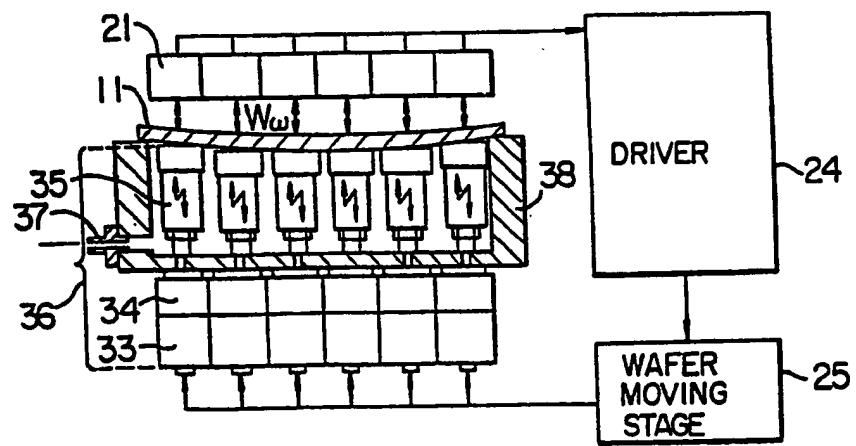


FIG. 7a

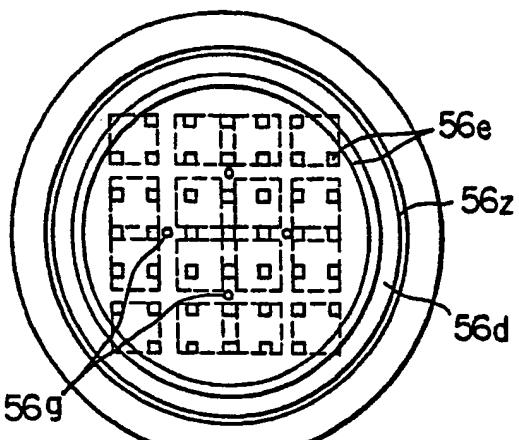


FIG. 7b

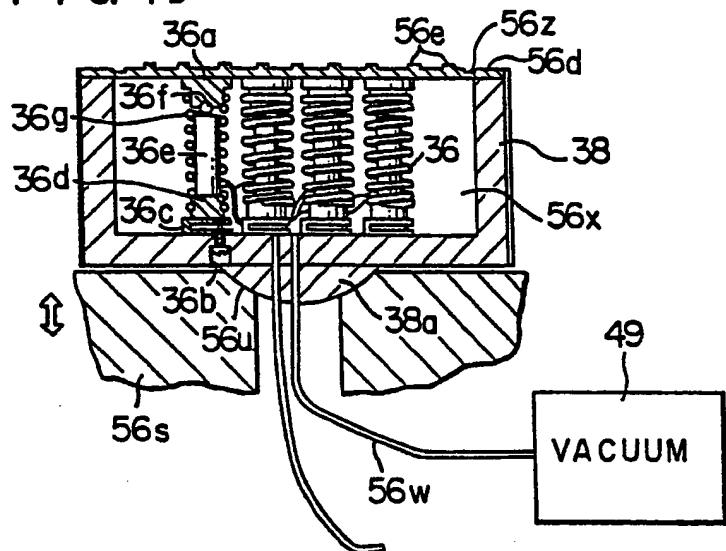
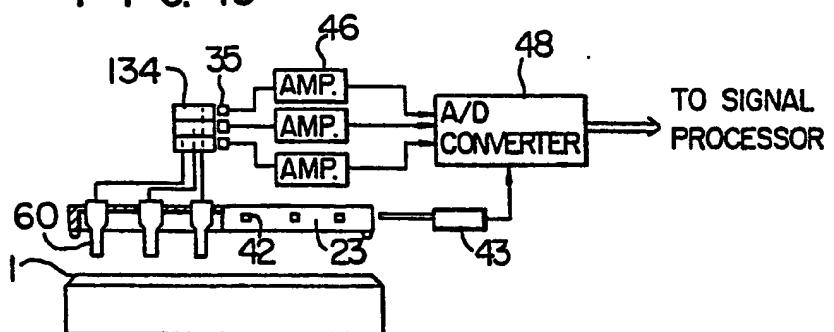
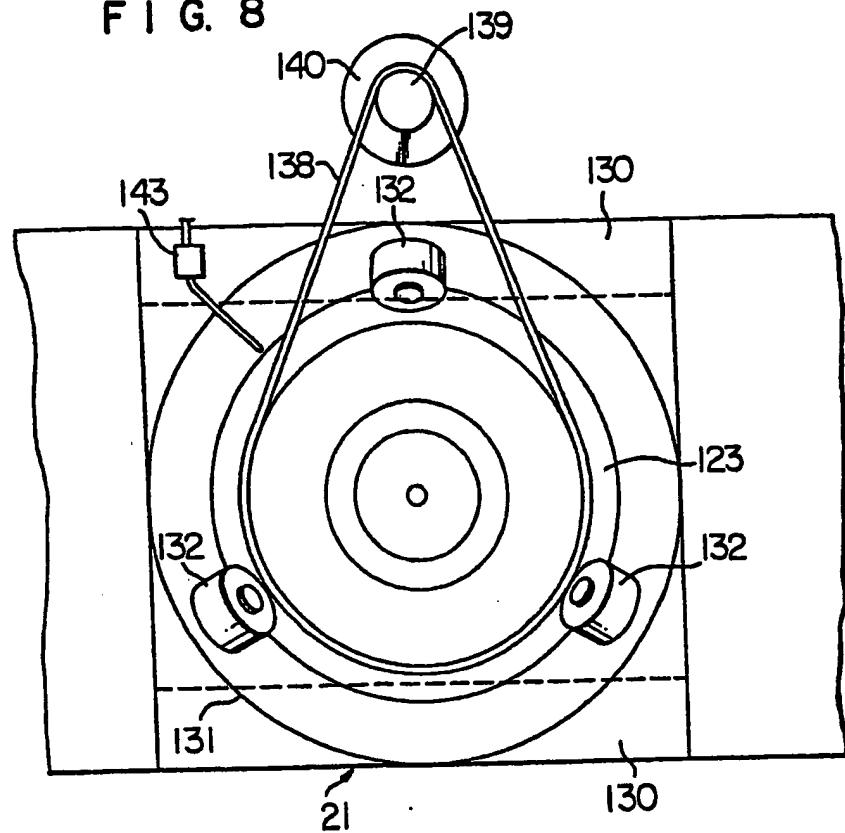


FIG. 10



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F I G. 8



F I G. 9

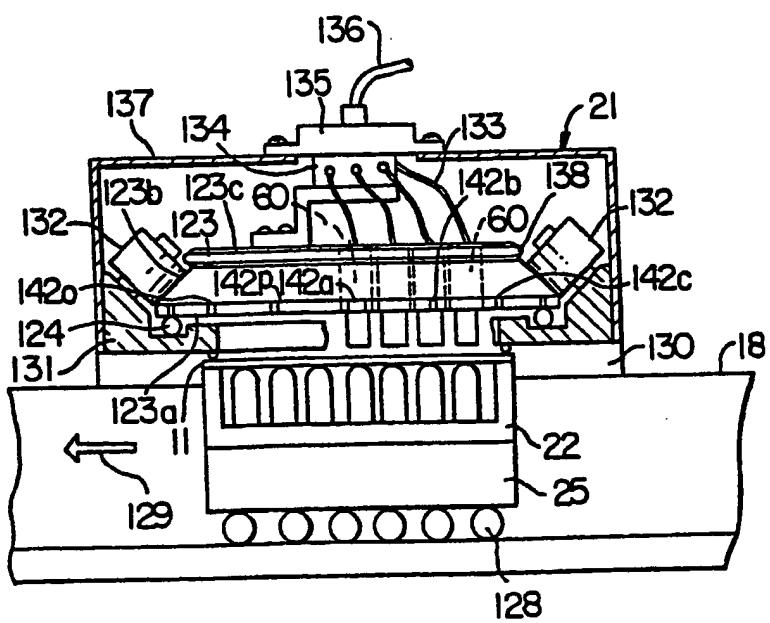


FIG. 11

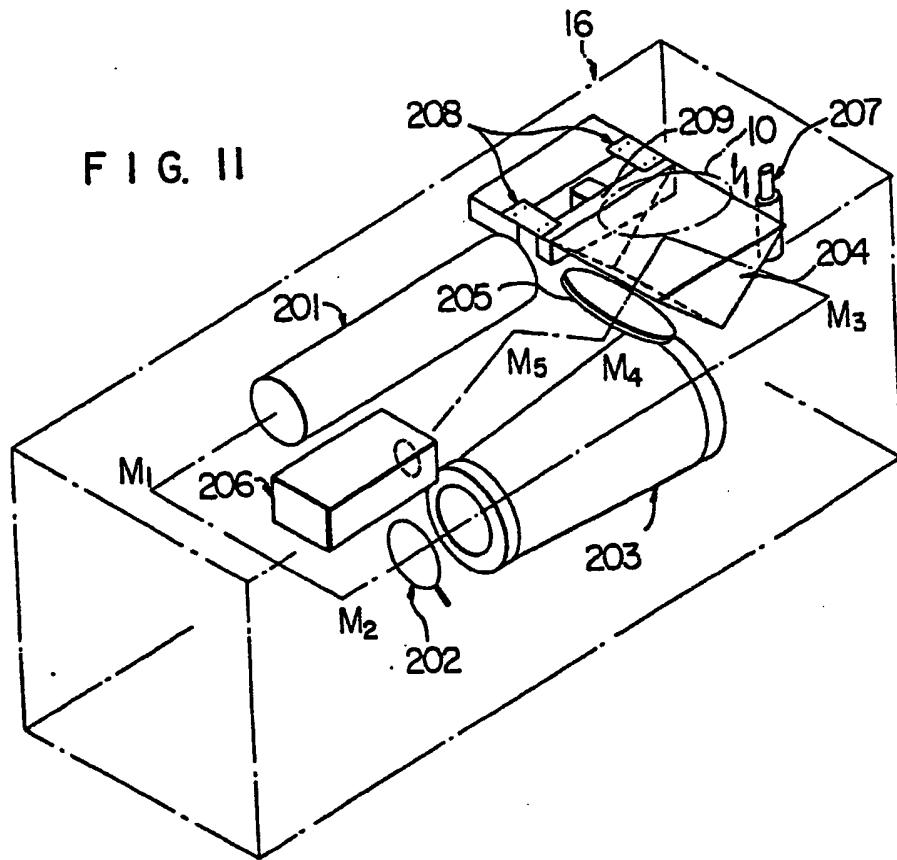
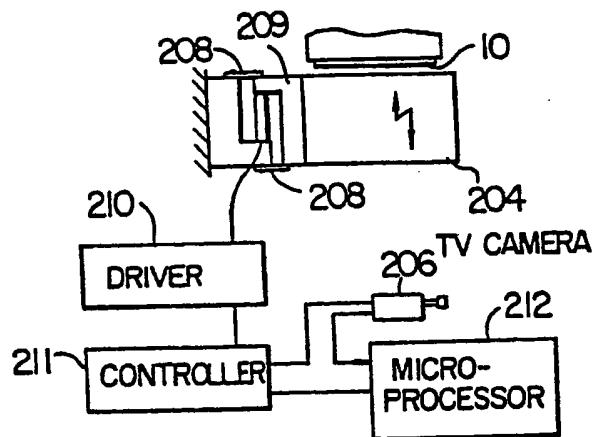
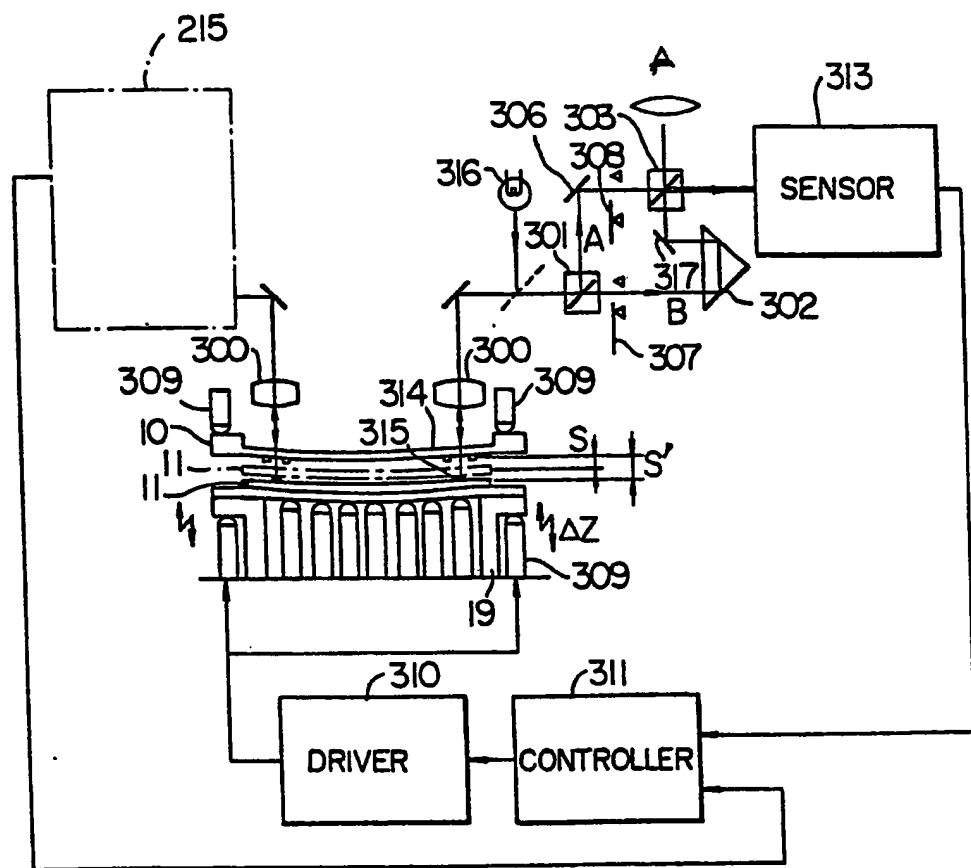


FIG. 12



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FIG. 13



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